

Yaldhurst Park
Yaldhurst
Christchurch

Submitted to:

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1 Introduction

ENGEO Ltd was requested by Infinity Yaldhurst Limited to undertake a Geotechnical Investigation - Stage 2 - 6 for the proposed 191 lot subdivision as outlined in our proposal (ref: P2018.001.727, dated 5 October 2018).

The property at Yaldhurst Park is located south of Yaldhurst Road, and is currently a partially developed subdivision. The purpose of this investigation was to comment on the suitability of the site for residential subdivision, and address the requirements of Section 106 of the Resource Management Act (RMA). To accomplish this, we have developed a geological model of the site, assessed the likely future land performance, and provided recommendations for subdivision works with preliminary geotechnical recommendations related to the design of foundations for typical timber framed residential dwellings.

Our overall scope for the site was to assess and provide geotechnical guidance related to the proposed development of 191 residential lots in two separate stages, diversion of the existing stream, and provide guidance related to stormwater basin design.

As requested by Infinity Yaldhurst Limited, we provided a specific assessment for Stage 1 of the works, which included geotechnical guidance related to the proposed development of 41 residential lots (blue outline in subsequent figures in this report) dated 9 November 2018 (reference 15518.000.000_01). The Stage 1 geotechnical report should be read in conjunction with this report.

Our geotechnical assessment for the remaining 150 lots that are located within Stages 2 through 6 (Figures 2 & 3), comments on the geotechnical aspects of the diversion of the existing stream, and guidance related to the stormwater basin design is provided within this report.

Our scope of works for Stages 2 through 6 included the following:

- Complete a desktop study of relevant available geotechnical and geological publications, including the New Zealand Geotechnical Database.
- Visit the site and undertake a geotechnical site walkover.
- Organise and technically supervise the excavation up to 30 test pits and associated Scala
 penetrometer and Shear Vane tests to a maximum depth of 3 m below ground level (or to
 native gravel) including geotechnical logging of the exposed soils, to assess the near surface
 material types and strength characteristics.
- Organise and technically supervise the drilling of up to four machine boreholes with SPTs at 1.5 m intervals to a target depth of 10 m below ground level. This includes geotechnical logging of the core to assess the deep soil types, strength characteristics and ground water depth, (as applicable).
- Preparation of this report outlining our findings on the ground conditions, and the suitability of
 the site for residential subdivision of Stages 2 to 6 (150 lots). This includes provision of
 geotechnical advice on the likely foundation Technical Category, conceptual foundation
 recommendations for typical timber-framed residential dwellings, and an assessment of the
 likely Geohazards required by Section 106 of the RMA.



2 Site Description

The development covers approximately 16.1 hectares including proposed parks, reserves, roads and existing waterways (Figure 1).

Stages 2 to 6 (approximately 11.8 hectares) is bound by an existing residential development south of the site, lifestyle blocks and farmland west of the site, and further residential development to the north and east of the site. Sir John McKenzie Ave, which was previously formed during prior subdivision development, intersects the subdivision. Stage 1 is outlined in blue as the area which has been previously assessed and has a geotechnical report issued (as outlined in Section 1).

The predominantly flat, to gently undulating site is partially developed land with stockpiled silt, fill, and unknown material observed in areas '1C' and areas '5A', '5B' and '5C' on the southern and eastern sides of the proposed development (Figures 2 & 3).

A stream, on the south-western corner of the site, is planned to be diverted during earthworks. Geotechnical recommendations for stream diversion are outlined in following sections of this report. Parks and areas of recreation are planned to run adjacent to the stream and beneath the row of electrical pylons intersecting the proposed subdivision (Figure 2). There are no significant watercourses mapped within the vicinity of the proposed development area.



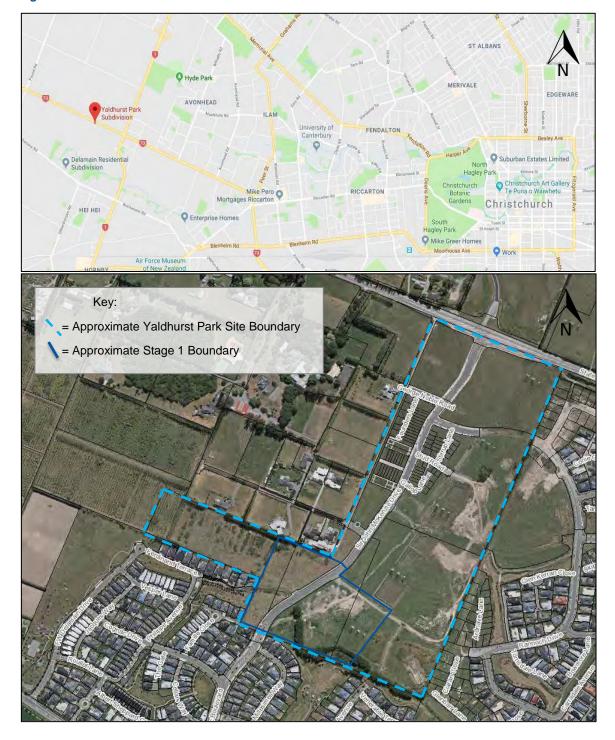


Figure 1: Site Location and Subdivision Plan

Image sourced from Canterbury Maps. Not to scale.



3 Development Proposal

Based on the Graham Surveying Limited Subdivision plans dated June 2018 (drawing number: GSL18036-CS-001 and GSL18036-CS-002) we understand that it is intended to subdivide stages 2 to 6 into 150 residential lots with multiple areas of recreation (Figure 2 and Figure 3). Lot sizes vary between 305 m² to 1520 m². A stream with associated recreation and park areas intended for public use will be incorporated within the development footprint.

We anticipate that future earthworks at the site for the residential development in Stages 2 to 6 will be limited to minor cut and fill to form building platforms and access ways. We anticipate moderate cut and fill to remove the stock piles of fill in stages 1C, 5A, 5B and 5C, to divert and form the proposed new stream location in stages 1B and 5C, to backfill the existing stormwater retention basin in stage 5C, and excavate the proposed stormwater basins on the western side of Stage 2.

Future buildings are anticipated to comprise conventional lightweight, timber framing and roof elements over a maximum of two-storeys.



Figure 2: Proposed Subdivision Development – Stages 1, 2, 3 and 5 (Stage 1 outlined in blue)

Image sourced from Graham Surveying proposed plans (Ref: GSL18036-CS-001 dated, 26 June 2018). Not to scale.





Figure 3: Proposed Subdivision Development – Stages 4 and 6

Image sourced from Graham Surveying proposed plans (Ref: GSL18036-CS-002 dated, 26 June 2018). Not to scale.

4 Published Geotechnical Information

4.1 Regional Geology

The site has been regionally mapped by Brown and Weeber (1992) as being underlain by dominantly alluvial sand and silt overbank deposits (Figure 4) and by GNS (Forsyth et al., 2008) as being underlain by river alluvium.



N

SPY

SPY

SPY

SPY

SPY

Approximate Yaldhurst Park Site Boundary

Approximate Stage 1 Boundary

Figure 4: Site Geology

Image sourced from Google Earth with the Brown and Weeber (1992) map overlay sourced from the New Zealand Geotechnical Database (NZGD). Not to scale.

4.2 CERA Land Classification

The Canterbury Earthquake Recovery Authority (CERA, now disestablished) has categorised the site as 'N/A Urban Non-residential', meaning future development can proceed following normal consenting processes. While the site itself does not have a specific technical classification (TC) as it is not zoned residential, nearby residential sites are classified as TC1 where "future land damage from liquefaction is unlikely", and "shallow soil strength testing which is standard for all homes" is required (Figure 5).



¹ SPY = Dominantly alluvial sand and silt overbank deposits

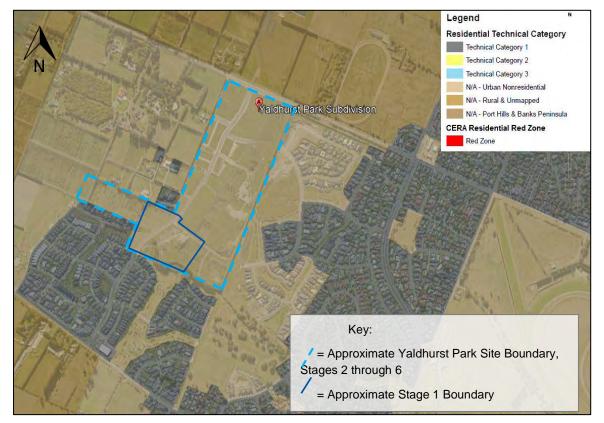


Figure 5: MBIE Residential Technical Categories Overlay

Image sourced from Google Earth with the MBIE Residential Technical Categories map overlay sourced from the New Zealand Geotechnical Database (NZGD). Not to scale.

4.3 New Zealand Geotechnical Database

Subsurface and Earthquake Specific Data

We have reviewed the NZGD and summarised the data relevant to this site in Tables 1 and 2. Publicly available nearby deep testing is summarised in Table 1 and with the location of this testing depicted in Figure 6.

Table 1: Summary of Near Site Investigations

CPT / Borehole Identifier	Position Relative to Site	Depth of Exploration (m)
BH_112631	100 m to the north	6.08
TP_93731	100 m to the north	2.7
TP_93730	100 m to the north	2.6
BH_72200	500 m to the south	5.27



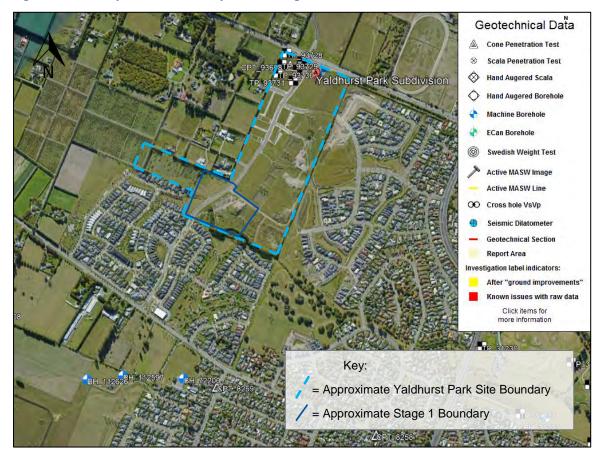


Figure 6: Publicly Available Near-by Site Investigations

Image sourced from Google Earth with the Surrounding Investigation Data map overlay sourced from the New Zealand Geotechnical Database (NZGD). Not to scale.



Table 2: Summary of Earthquake Specific Data

	Events			
	4 Sept 2010 (Mw 7.1)	22 Feb 2011 (Mw 6.2)	13 Jun 2011 (Mw 6.0)	23 Dec 2011 (Mw 5.9)
Median PGA (g)	0.28	0.23	0.12	0.12
PGA Probable Range (g)1	0.17 to 0.41	0.13 to 0.35	0.07 to 0.19	0.07 to 0.19
PGA7.5 (g)2	0.25	0.16	0.08	0.08
170% of SLS	Sufficient	Not Sufficient	Not Sufficient	Not Sufficient
10th Percentile >SLS	Sufficient	Sufficient	Not Sufficient	Not Sufficient
Liquefaction and Lateral Spreading Observations (EQC)	No observed liquefaction ejecta (road observations)	No observed liquefaction ejecta (road observations)	No observed liquefaction ejecta (road observations)	No data available
Site Specific Aerial Photograph Liquefaction Interpretation3	No data available	No obvious evidence of liquefaction ejecta at the site or the surrounding area	No data available	No data available
Mapped Ground Cracks	No mapped cracks on site, or mapped within 150 m of the site.			

¹Range for one standard deviation either side of the mean.

Groundwater

Groundwater has been regionally mapped by both GNS Science (GNS) and EQC to be greater than 6 m below the ground surface at the time of the 2010 - 2011 Canterbury earthquake sequence. The closest measurement well is approximately 1.5 km west and 1.5 km north of the site.

LiDAR and Ground Movement

EQC has prepared maps showing the change in surface elevation and horizontal deformation, as measured by a series of aerial LiDAR surveys. GNS has created a "dislocated tectonic contour model" which shows the tectonic uplift or subsidence on a regional level based on survey of discrete benchmarks on bedrock outcrops across the Canterbury region. Subtracting the tectonic component of vertical deformation from surveyed ground levels gives an indication of vertical deformation from soil subsidence.



²Using Idriss and Boulanger (2008) magnitude scaling factor.

³Interpreted by ENGEO.

LiDAR maps prepared for the EQC generally show a cumulative subsidence of approximately up to 100 mm across the site.

4.4 Historic Aerial Photography

We reviewed limited aerial photographs of the site dating back to 1941 and describe relevant observations below:

- Prior to 1941, the site appears to have been developed with a track for horse training and outside of the horse training track has been used for agricultural purposes. The stream locations observed in the 1941 aerial photography, appear to be in the same locations as present.
- Between 1941 and 1950, the size of the horse racing track increased (Figure 7).
- Between 1960 and 1970, a row of pylons had been constructed in the same location as the present location.
- Between 1980 and 1990, the site had been developed into an orchard (Figure 8).
- Between 2000 and 2011, the site had been cleared and the development begun for the existing subdivision.

Figure 7: 1950 Aerial Photography

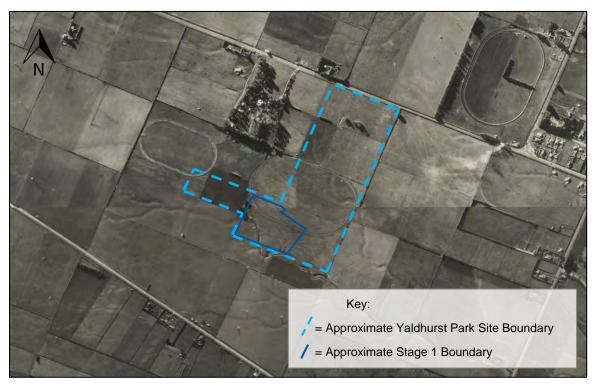


Image sourced from Canterbury Maps with the 1950 aerial photo overlay. Not to scale.



Figure 8: 1990 Aerial Photography

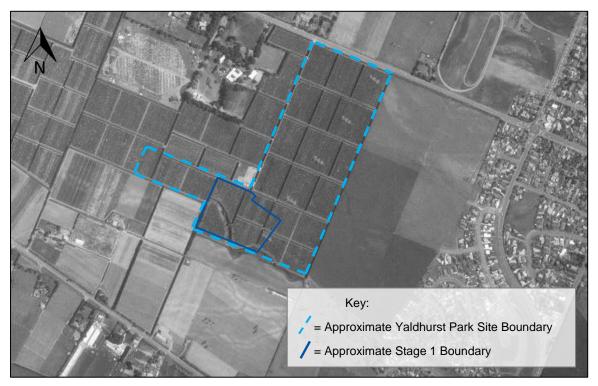


Image sourced from Canterbury Maps with the 1990 aerial photo overlay. Not to scale.

Figure 9: 2011 Aerial Photography

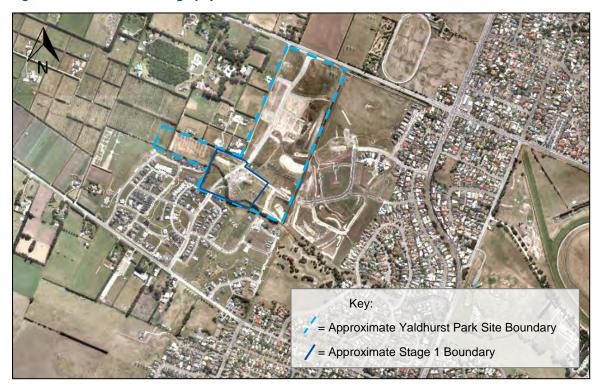


Image sourced from Canterbury Maps with the 2011 aerial photo overlay. Not to scale.



4.5 Minimum Floor Levels for Flood Mitigation

The Christchurch City Council (CCC) and CERA have released updated recommended floor levels for flood avoidance for properties in the Avon, Heathcote and Styx river catchments, as well as Sumner. The site is located outside the "CCC City Plan – Flood Management Area", and specific floor level recommendations are not provided by the Council. CCC should be contacted for specific floor level elevations related to the site prior to finalised development.

5 Site Investigation

ENGEO visited the site on 24 October and 23 November 2018 and made the following observations which are also depicted in photographs presented in Figure 10:

- The subdivision is currently partially established from the work completed by a previous developer. Some formed roads, partially formed roads, partially formed lots, public recreation areas and stormwater basins (Photo 1) have been constructed.
- A stream is running east to west on the southern side of Stage 1 and Stage 5C of the
 development, and the base of the streambed is approximately 1.5 m below adjacent ground
 level (Photo 1). Approximately 200 mm to 400 mm of water was observed in the base of the
 stream at the time of our site visit. We understand that the stream is planned to be diverted
 during the earthworks stage of development.
- A row of electrical pylons run through the proposed development with retention basins constructed adjacent to the pylons (Photo 2 and depicted in Figure 2 & 3)
- In the area of Stages 1C, 5A, 5B and 5C a series of fill, silt and unknown material stockpiles were observed (Photos 3 & 4). Through discussions with the client, these stockpiles are to be removed or re-used (depending on soil type) during the proposed earthworks and development of the site.
- In Stage 2 a series of stockpiles of organic material and unknown material stock piles were observed (Photo 5). Through discussions with the client, these were likely the old orchard trees which were removed and stockpiled. An existing orchard was observed in the northeastern most corner of Stage 2.
- In Stage 4 and Stage 5B, localised areas of contaminated soils were flagged by a previous environmental consultant (Figure 11). At the request of the client, we avoided these areas during our subsurface investigation.
- In the south-eastern corner of Stage 5C we observed an existing stormwater retention basin
 excavated approximately 2.5 m to 3 m below adjacent ground level (Photo 6). Through
 discussions with the client, it is proposed to fill this basin with engineered fill during the
 earthworks stage of this project.
- No obvious evidence of lateral stretch across the site was observed during our site visit.
 However, owing to the vegetation, stock piles, soft soil and machine activity on-site, minor ground cracks could have been concealed.
- No obvious signs of earthquake-induced land damage such as lateral spreading, sand boils
 or other features that we would associate with liquefaction, or fault rupture was observed at
 the time of our site visit.

Site photographs are presented in Figure 10.



Figure 10: Site Photographs



Photo 1: Stage 1 of Yaldhurst Park Subdivision development. Stream described above in the foreground (black arrow).



Photo 2: Electrical pylons observed to intersect the subdivision development. Existing storm water retention basins adjacent to the pylons (black arrow).



Photo 3: Silt, fill and unknown material stockpiles observed in Stages 1C, 5A, 5B and 5C of the development. Row of electrical tower pylons with adjacent stormwater retention basins observed.



Photo 4: Areas of stockpiled fill within Stage 5B. Stock piles are overgrown and the material type is unknown.



Photo 5: Organic and unknown stockpiles observed in Stage 2 of the development. The client indicated these are likely to be old orchard trees.



Photo 6: Stormwater retention basin observed in Stage 5C approximately 2.5 to 3 m below adjacent ground

6 Subsurface Investigation

ENGEO completed a site investigation on 24 October 2018 to assess the shallow subsurface material types and strength characteristics within Stages 2 to 6 of the Yaldhurst Park Subdivision Development. The investigations comprised of 30 test pit investigations with associated Scala penetrometer tests to assess the near surface soil types and strength characteristics.

We also completed site investigation to assess the deep subsurface materials on 23 November 2018 to 27 November 2018 which comprised of four machine boreholes drilled to a target depth of 10 m with 1.5 m SPT's to assess the soil types, strength characteristics and ground water depth (if applicable).

The locations of all tests are shown in Figure 11 (and Appendix 1) and our findings are detailed in the following sections.



Figure 11: Site Investigation Locations

The investigations revealed subsurface conditions across the site are consistent with the published geological mapping, as summarised in Table 3.



Depth to top **Layer Thickness** Density / **Soil Type** Comment of layer (m) (m) Consistency Firm to Stiff / Loose to TOPSOIL / FILL 0.0 0.2 to 0.5 Medium Dense Varies between silt and Stiff to Very Stiff / SILT / SAND 0.5 1.5 to 2.4 sand depending on test Loose to Dense pit location Medium Dense to Very Sandy GRAVEL 2.0 to 10.91* Unknown Dense (inferred from SPT results)

Table 3: Generalised Summary of Subsurface Conditions

Subsurface profile below approximately 2.9 m inferred from the machine boreholes.

No standing water was observed in any of the test pit excavations. Standing water was observed between 7.5 m bgl in BH02 and 9 m bgl in BH03. In both BH01 and BH04, no standing water was observed within the depth drilled, 10.91 m.

Test pit and borehole locations are shown in Figure 10 and in the Site Plan presented in Appendix 1. Test pit logs, showing detailed soil descriptions are presented in Appendix 2. Borehole logs, showing detailed soil descriptions are presented in Appendix 3.

6.1 ECan Boreholes

A review of five deep ECan borehole logs located onsite, M35/5721, M35/11334, M35/11335, M35/11336 and M35/11338 was conducted (Canterbury Maps). The location of these boreholes is presented in Figure 12 and includes well points that have no log data available. The logs from all five holes of interest are presented in Appendix 3 and indicate the site is underlain by gravel and sandy gravel with thin slit and clay layers to depths of at least 15 m below ground level.

6.2 ECan Groundwater

Groundwater is recorded in the surrounding ECan boreholes between approximately 13.9 m and 14.9 m depth. These ground water depths are a function of the slotted depth of the wells installed for groundwater well pumping, and do not necessarily represent the actual groundwater depth at the site.





Figure 12: Nearby ECan Borehole Locations

Image sourced from Canterbury Maps (November 2018). Not to scale.

6.3 Site Seismic Class

In accordance with NZS 1170.5:2004, site classification "Class D" applies to this particular site, defining it as a 'deep soft soil site'.

7 Liquefaction Assessment

7.1 Canterbury Earthquake Sequence Ground Shaking

Bradley and Hughes (2012) have developed a contour map of the conditional median peak ground accelerations (PGA) interpolated from data measured at various recording stations during the 2010 - 2011 Canterbury earthquake sequence. The PGA contour map was created by combining the prediction from an empirical ground motion model of the fault rupture with the PGA recorded at strong motion sites. The conditional median PGA experienced at the site during the major Christchurch earthquake events using the published contour mapping are presented in Table 2.



Based on the model by Bradley and Hughes (2012), and earthquake magnitude scaling to M7.5, we can conclude that the site, under the 10th percentile test, has undergone more than 170% of the serviceability limit state (SLS) level seismic event for the September 2010 and February 2011 earthquake event. According to Appendix D1 of the MBIE Guidance, the site can therefore be regarded as having been sufficiently tested for a SLS event.

7.2 Liquefaction and Lateral Spreading Analysis

For comparison to the "index values" in the MBIE Guidance document, we performed liquefaction analyses using on-site SPT (borehole) data and based on the liquefaction triggering methodologies presented by Boulanger and Idriss (2014). For the SLS and ULS events, from our site investigation, a conservative groundwater depth of 7 m was used for the analysis.

The main input parameters used in our assessment include the following:

- Three ground motions (2 SLS motions, and 1 ULS motion) as outlined below:
 - ULS = PGA of 0.35 g / Magnitude of 7.5
 - o SLS Case 1 = PGA of 0.13 g / Magnitude of 7.5
 - o SLS Case 2 = PGA of 0.19 g / Magnitude of 6.0
- A probability of liquefaction triggering curve (PL) of 15% (deterministic curve).

Liquefaction analyses are included as an attachment to this document and calculated settlements are summarised in Table 4. We note that the settlements provided are for an undeveloped site and that settlements beneath the dwelling are likely to be greater.

Table 4 presents the results of our liquefaction analysis under ULS and SLS loading.

Table 4: Summary of Liquefaction and lateral spreading analysis

Decision Cons	Calculated Vertical Settlement ¹		
Design Case	Total	Upper 10 m	
ULS	<10 mm	<10 mm	
SLS	<10 mm	<10 mm	

¹For an undeveloped site. Settlements beneath buildings are likely to be greater.

Due to the groundwater depth and ground conditions observed in our geotechnical investigation, we anticipate that liquefaction is unlikely to occur under SLS level and ULS earthquake ground motions. Calculated vertical settlements in the upper 10 m were estimated to be less than 10 mm under both SLS and ULS.

The analysis considers volumetric strain and does not account for ground loss due to ejecta. Owing to the thickness of the non-liquefiable layer above the ground water level (7 m), the minimal liquefiable layers and potentially liquefiable material below the groundwater table, sand boil formation and ejecta are unlikely to occur at the site under both SLS and ULS shaking.

The liquefaction analysis is attached to this report.



7.3 Technical Classification – Stages 2 to 6 of Yaldhurst Park Development

Based on our site investigation and observations, and owing to the nature of the subsurface materials and depth to groundwater at the site, we consider the potential for liquefaction and lateral spreading to be low within Stages 2 to 6 of the Yaldhurst Park Subdivision.

We therefore consider that Stages 2 to 6 of the proposed subdivision to have Technical Category 1 (TC1) related to future land performance where by future land damage from liquefaction is unlikely, and ground settlements are expected to be within normally accepted tolerances.

8 RMA Section 106 Requirements and Suitability to Subdivide

Section 106 of the Resource Management Act 1991 states a consent authority may refuse to grant a subdivision consent, or may grant a consent subject to specific consent conditions if the land is likely to be subject to the following:

- Erosion, including surface and subsurface erosion, associated with water and wind.
- Falling debris, including rockfall that could impact the site from upslope sources.
- Subsidence, which involves the removal of underlying support by natural or artificial means.
- Slippage, which is defined as the downslope transfer of materials by sliding and / or flowage.
- Inundation, which may be sourced from streams, coastal processes or excess precipitation.

Based on our observations and the nature of the site, its performance during the CES, and the site's distance from the nearest significant watercourse, we consider it is unlikely for the site to be subject to any of the above hazards. As such, the site is considered suitable for subdivision from a geotechnical perspective.

9 Preliminary Geotechnical Recommendations

9.1 Earthworks

For planning purposes, structure footprints should be set back at least 10 m from any water course. Earthworks carried out for the subdivision shall be in accordance with NZS 4404:2010, Land Development and Subdivision Infrastructure and NZS 4431:1989, Code of Practice for Earthfilling for Residential Development. In particular, any areas to receive fill should be stripped of any vegetation, topsoil, non-engineered fill, soft or organic soils prior to fill placement.

Fill may comprise clean natural sandy gravel, sandy or silty soils, or clean imported soils and / or granular fill, compacted to achieve no less than 95% of maximum dry density. Fill faces steeper than 2:1 (horizontal to vertical) and higher than 600 mm should be retained or specifically designed and referred back to ENGEO. Although unlikely, where any springs or groundwater seeps are encountered, they should be intercepted with suitable drainage and discharged to a Council approved outlet.

A comprehensive earthworks specification should be provided to the earthworks contractor prior to starting excavations and an inspection / testing regime agreed, along with a robust erosion and sediment control plan.



9.2 Stream Diversion

Where the stream in planned to be diverted, directly effecting Lots 105 and 106, any soft, wet, and organic soils should be removed prior to placement of engineered fill. The engineered fill should be benched into the sides of the former stream bank and the differential fill thickness under specific building footprints should be less than 1.5 m.

We will provide a subsequent document with specific earthworks recommendations for the proposed diversion of the stream.

9.3 Stormwater Retention Basin Design

All unretained batters of pond and stormwater drains constructed with the native silty, sandy, or sandy gravel material should be at an inclination no steeper than 1V:3H, with protection schemes in place to control erosion of the formed batters within the waterways.

A comprehensive earthworks specification should be provided to the earthworks contractor prior to starting excavations and an inspection / testing regime agreed, along with a robust erosion and sediment control plan.

9.4 Subdivision Roading

Vegetation, any organic or deleterious material, topsoil and non-engineered fill should be removed from under pavement areas prior to aggregate placement. Based on our observations during testing, we consider the native ground below the topsoil at the site should provide an adequate subgrade for the proposed pavement areas. However, specific testing of the roadway subgrade should be accomplished to provide CBR values that can be utilised for the design of the roadways

9.5 Stormwater Control

Concentrated stormwater flows from all impermeable areas must be collected and carried in sealed pipes to the Council system or an alternative disposal point subject to approval from Council. Uncontrolled stormwater must not be allowed to saturate the ground as this will potentially affect future foundation performance both statically and during future seismic activity.

9.6 Foundations

Foundations for future proposed residential dwellings within the subdivision may comprise pad, strip or slab foundations designed in accordance with the provisions of NZS 3604 Timber Framed Buildings.

For planning purposes, a preliminary geotechnical Ultimate Bearing Capacity of 200 kPa may be assumed for foundations bearing on native sandy or silty soils, or engineered fill, below any topsoil. We anticipate the bearing layer to be between 0.2 m to 0.5 m depth based on our subsurface investigations.

Lot specific testing as defined in Module 2 of MBIE Earthquake Geotechnical Engineering Practice (Nov 2016) should be accomplished as part of the design level geotechnical report to provide final foundation design recommendations as ground conditions may vary across the site. Subgrade conditions should be confirmed during construction by a suitably qualified geotechnical professional.



10 Additional Considerations

- A comprehensive earthworks specification should be provided to the earthworks contractor
 prior to starting excavations and an inspection / testing regime agreed, along with a robust
 erosion and sediment control plan.
- ENGEO should be given the opportunity to review the geotechnical aspects of the grading plan prior to submitting for Building Consent;
- ENGEO has been engaged to observe the excavations during construction to assess the suitability of the subgrade prior to placement of any fill, test fill for verification of compaction, and to assess that the recommendations presented in this report have been interpreted as intended.
- Lot specific subsurface testing as defined in Module 2 of MBIE Earthquake Geotechnical Engineering Practice (Nov 2016) should be accomplished as part of the design level geotechnical report to provide final foundation design recommendations.



11 References

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We also acknowledge the New Zealand GeoNet project and its sponsors EQC, GNS Science and LINZ, for providing data used in this report.



12 Limitations

- i. We have prepared this report in accordance with the brief as provided. This report has been prepared for the use of our client, Infinity Yaldhurst Limited, their professional advisers and the relevant Territorial Authorities in relation to the specified project brief described in this report. No liability is accepted for the use of any part of the report for any other purpose or by any other person or entity.
- ii. The recommendations in this report are based on the ground conditions indicated from published sources, site assessments and subsurface investigations described in this report based on accepted normal methods of site investigations. Only a limited amount of information has been collected to meet the specific financial and technical requirements of the client's brief and this report does not purport to completely describe all the site characteristics and properties. The nature and continuity of the ground between test locations has been inferred using experience and judgement and it should be appreciated that actual conditions could vary from the assumed model.
- iii. Subsurface conditions relevant to construction works should be assessed by contractors who can make their own interpretation of the factual data provided. They should perform any additional tests as necessary for their own purposes.
- iv. This Limitation should be read in conjunction with the Engineers NZ/ACENZ Standard Terms of Engagement.
- v. This report is not to be reproduced either wholly or in part without our prior written permission.

We trust that this information meets your current requirements. Please do not hesitate to contact the undersigned on (03) 328 9012 if you require any further information.

Report prepared by

Hamish Foy

Geotechnical Engineer

Report reviewed by

Don Bruggers, CMEngNZ (CPEng)

Principal Engineer

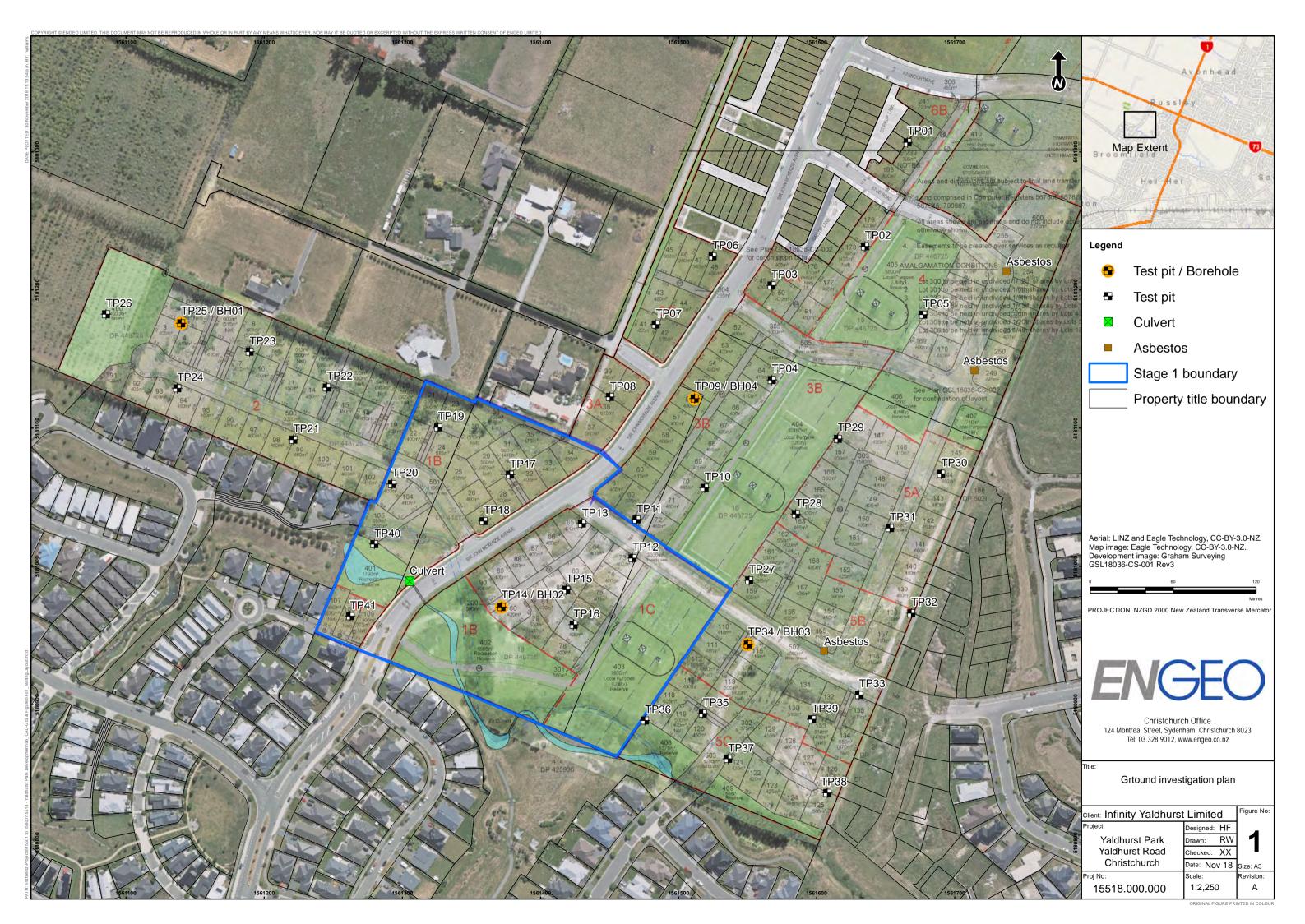




APPENDIX 1:

Testing Location Plan







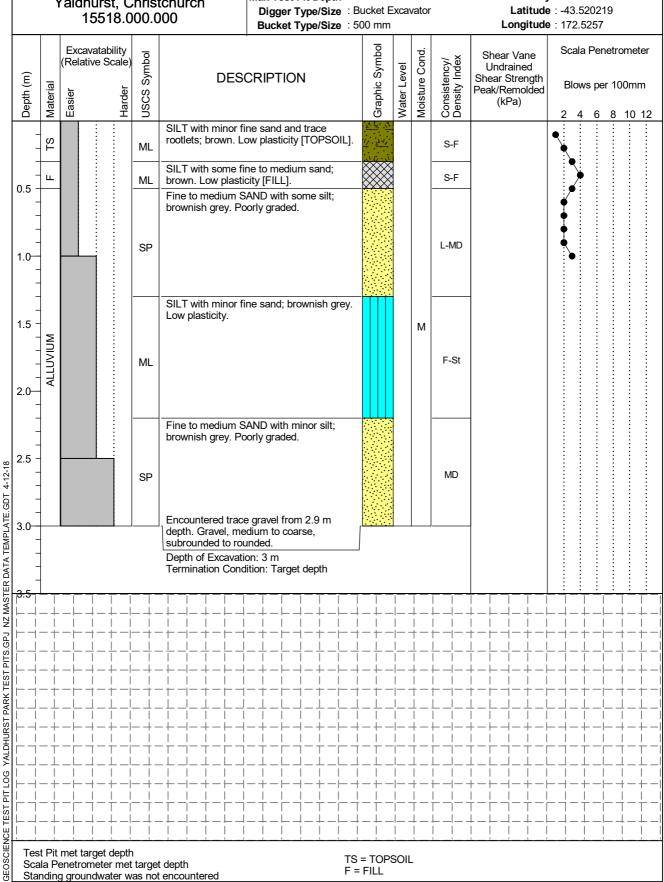
APPENDIX 2:

Test Pit Logs





Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000 Max Test Pit Depth : 3 m Reviews



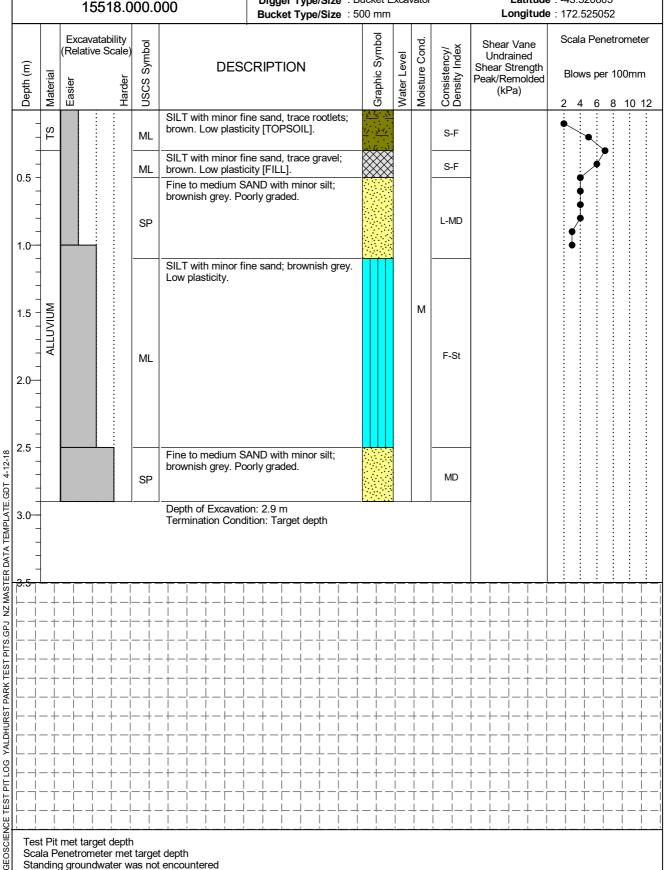


Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000

Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By : HB Date: 24/10/18

Max Test Pit Depth : 2.9 m Reviewed By: HF

Digger Type/Size : Bucket Excavator Latitude: -43.520803



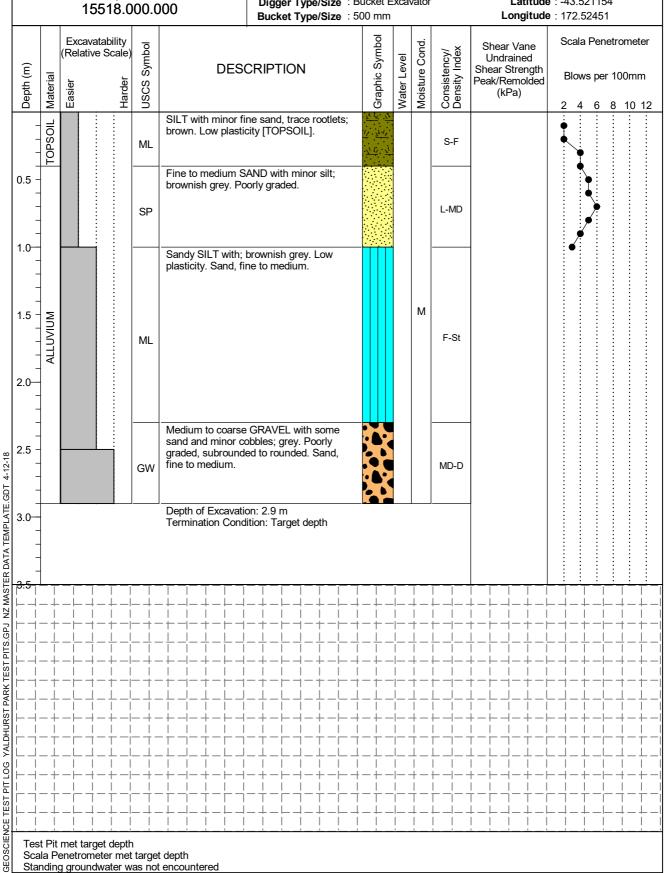


Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000

Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By : HB Date: 24/10/18 Reviewed By: HF

Max Test Pit Depth : 2.9 m

Digger Type/Size : Bucket Excavator Latitude: -43.521154 Longitude: 172.52451



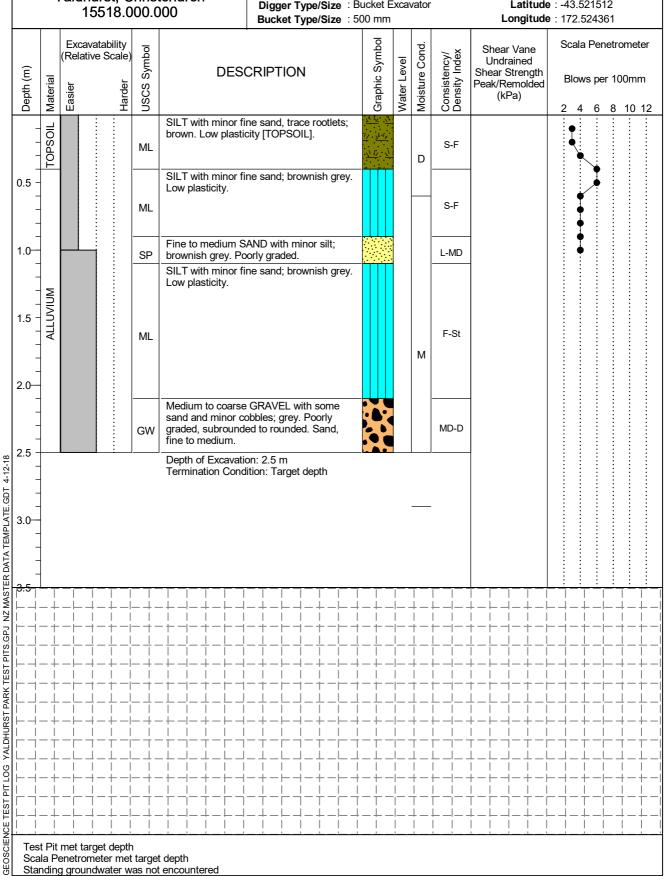


Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch

Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By : HB Date: 24/10/18 Reviewed By: HF

Max Test Pit Depth: 2.5 m

Digger Type/Size : Bucket Excavator Latitude: -43.521512 Longitude: 172.524361



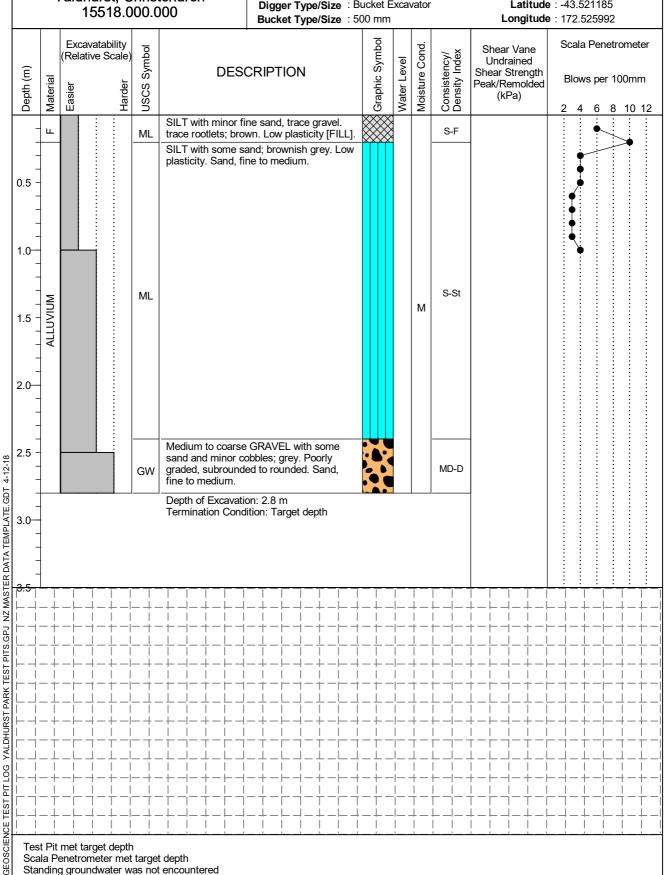


Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch

Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By : HB Date: 24/10/18 Reviewed By: HF

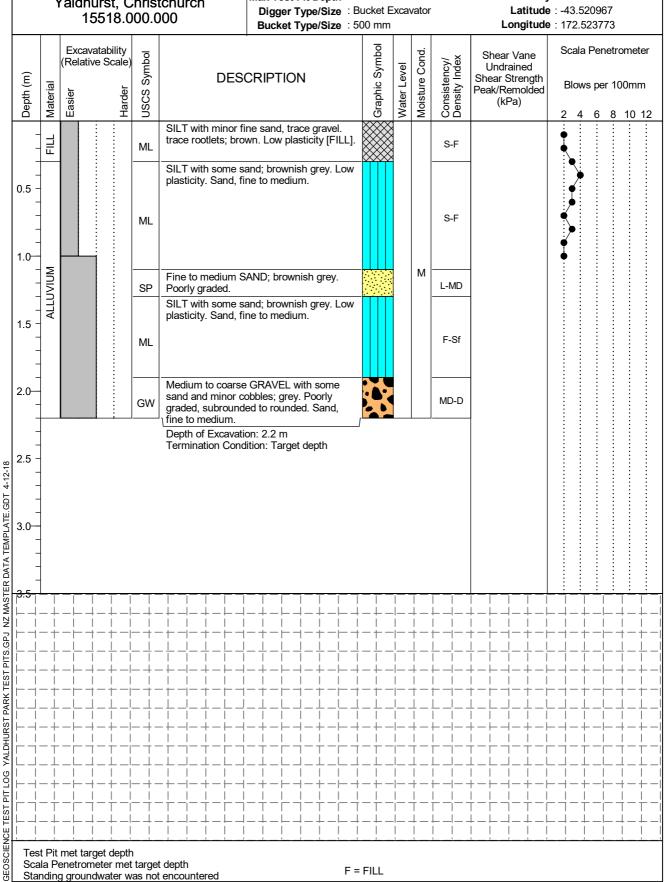
Max Test Pit Depth : 2.8 m

Digger Type/Size : Bucket Excavator Latitude: -43.521185





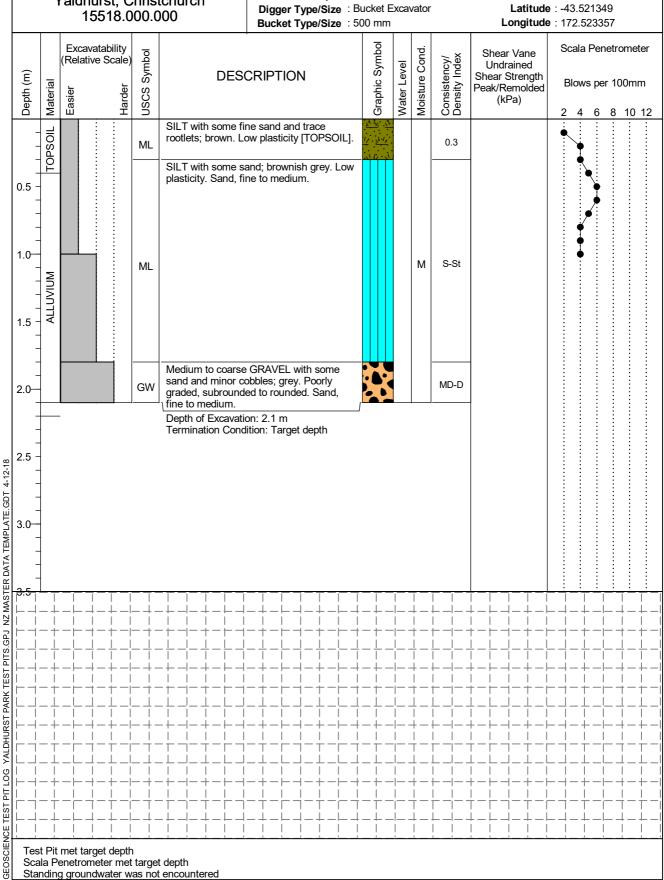
Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000





Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch

Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By: HB Date: 24/10/18 Max Test Pit Depth: 2.1 m Reviewed By: HF



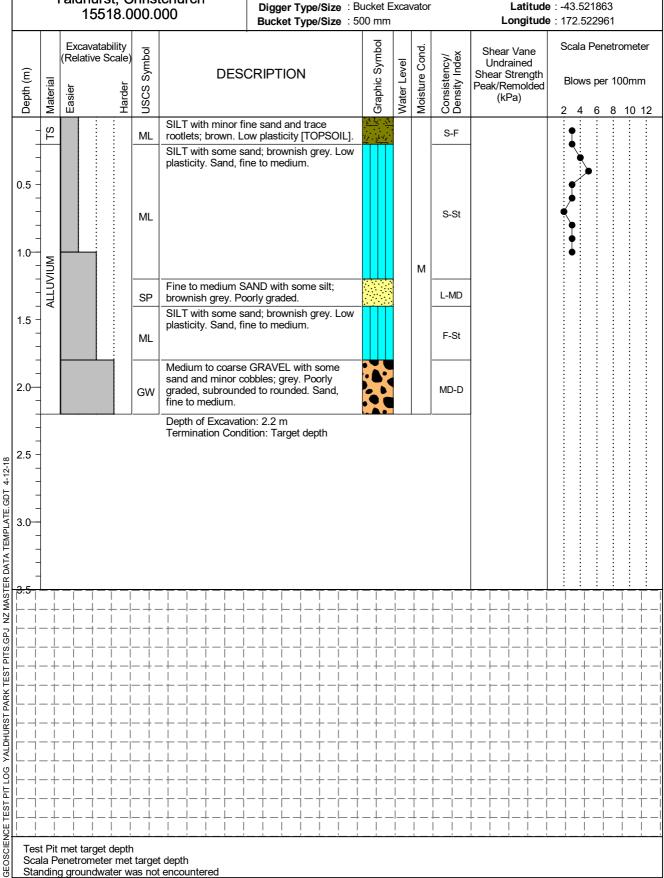


Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch

Shear Vane No: NA Client: Infinity Yaldhurst Limited Logged By: HB Date: 24/10/18 Reviewed By: HF

Max Test Pit Depth: 2.2 m

Digger Type/Size : Bucket Excavator

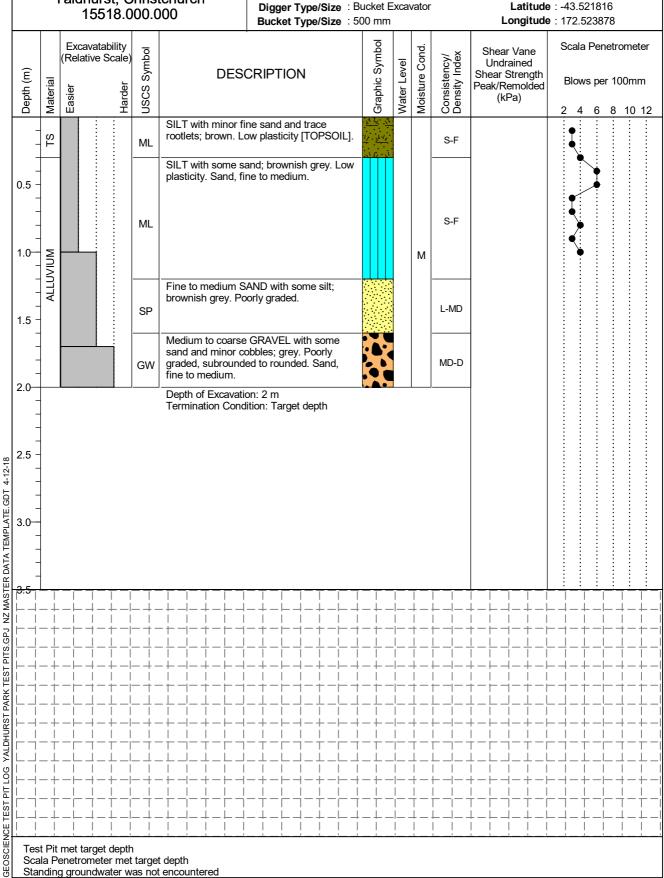




Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch

Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By: HB Date: 24/10/18 Reviewed By: HF

Max Test Pit Depth : 2 m



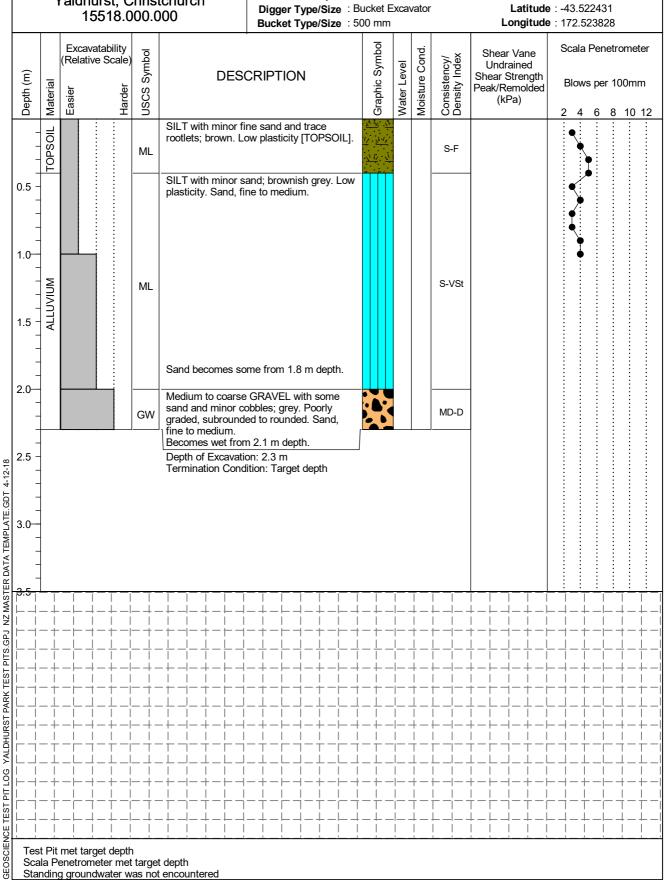


Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch

Shear Vane No: NA Client: Infinity Yaldhurst Limited Logged By : HB Date: 24/10/18 Reviewed By: HF

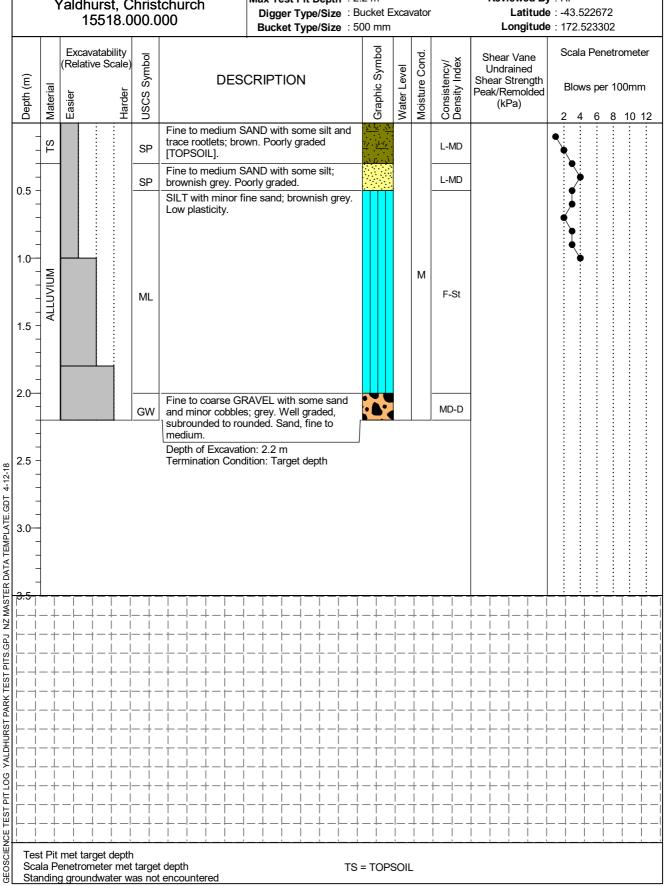
Max Test Pit Depth : 2.3 m

Latitude: -43.522431





Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000

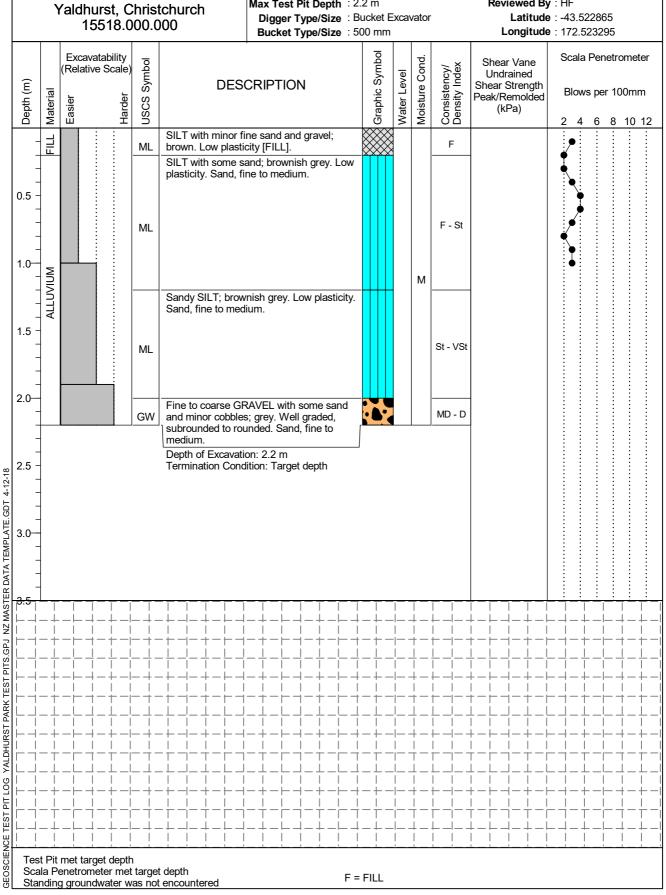




Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000

Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By : HB Date: 24/10/18

Max Test Pit Depth: 2.2 m Reviewed By: HF



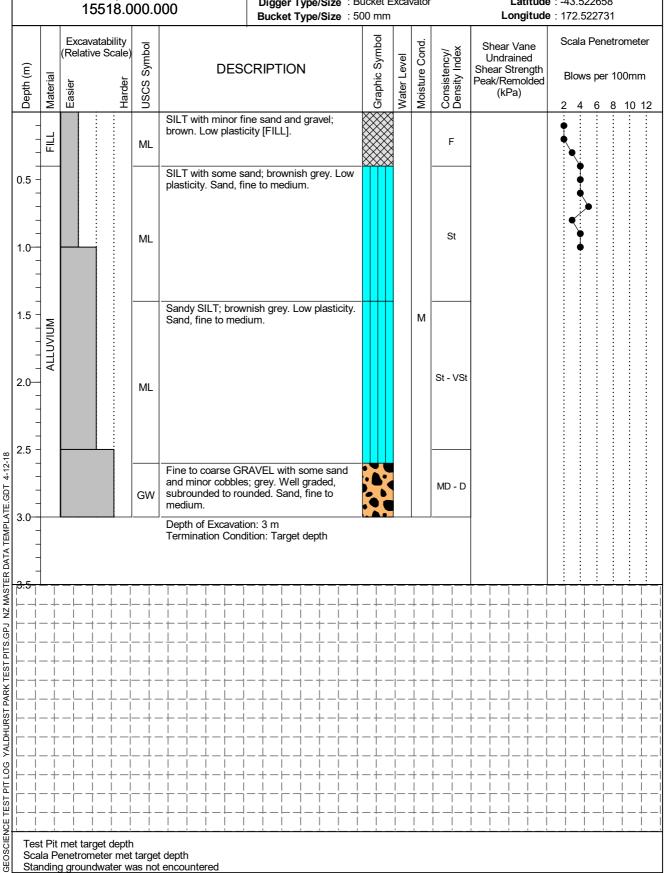


Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch

Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By : HB Date: 24/10/18 Reviewed By: HF

Max Test Pit Depth: 3 m

Digger Type/Size : Bucket Excavator Latitude: -43.522658 Longitude: 172.522731





Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000

Scala Penetrometer met target depth

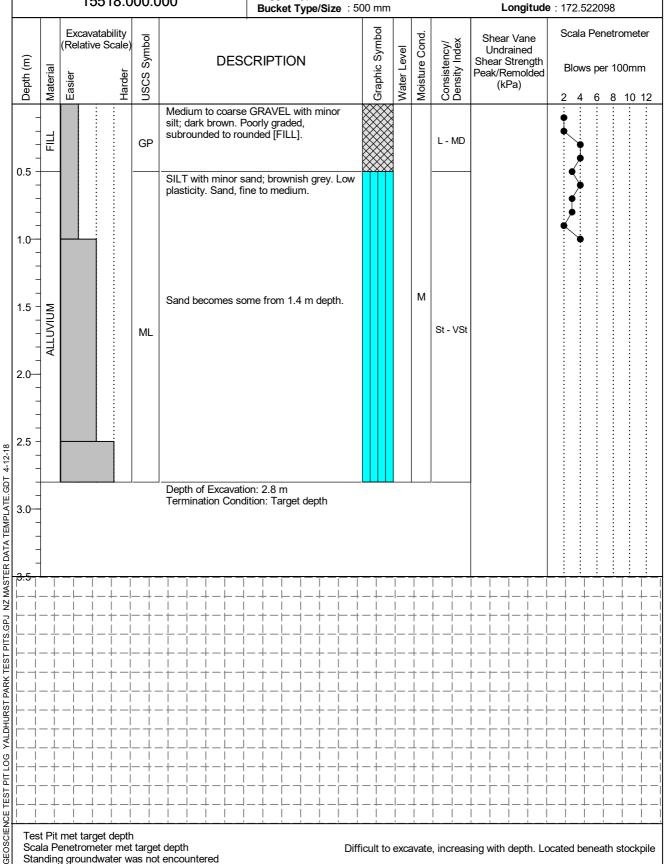
Standing groundwater was not encountered

Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By : HB Date: 24/10/18 Reviewed By: HF

Max Test Pit Depth : 2.8 m

Digger Type/Size : Bucket Excavator Latitude: -43.52309

Difficult to excavate, increasing with depth. Located beneath stockpile



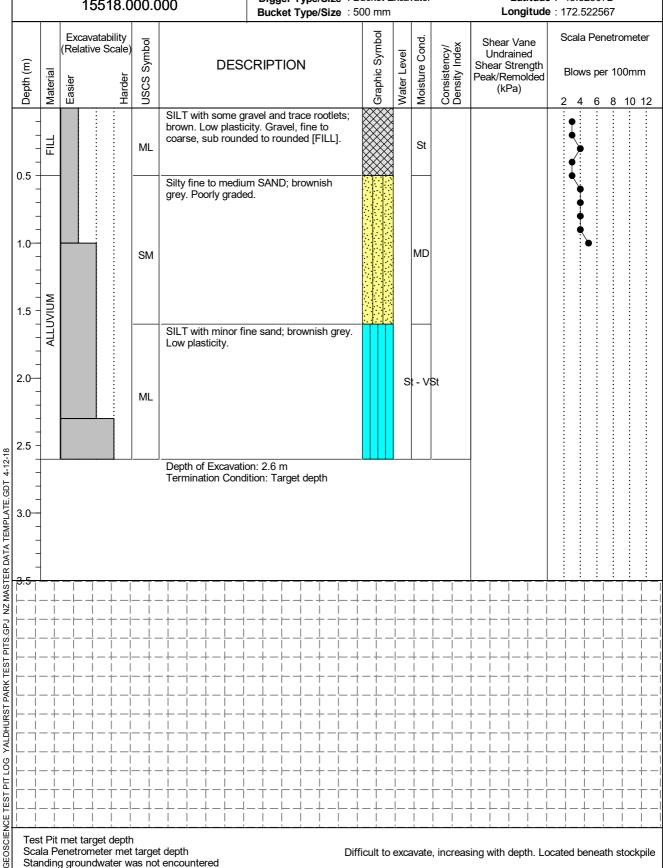


Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000

Standing groundwater was not encountered

Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By : HB Date: 24/10/18

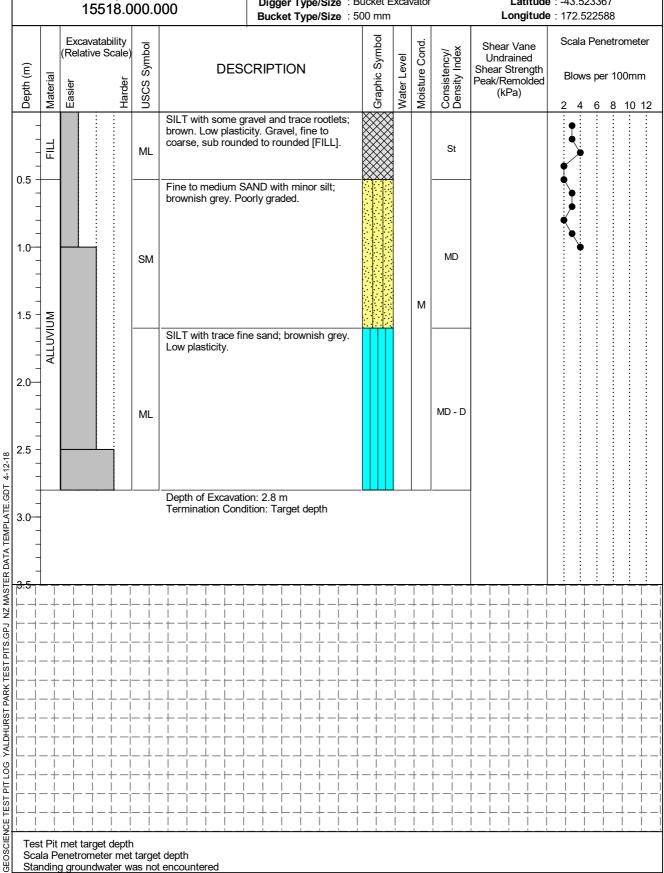
Max Test Pit Depth: 2.6 m Reviewed By: HF





Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000

Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By : HB Date: 24/10/18 Max Test Pit Depth: 2.8 m Reviewed By: HF

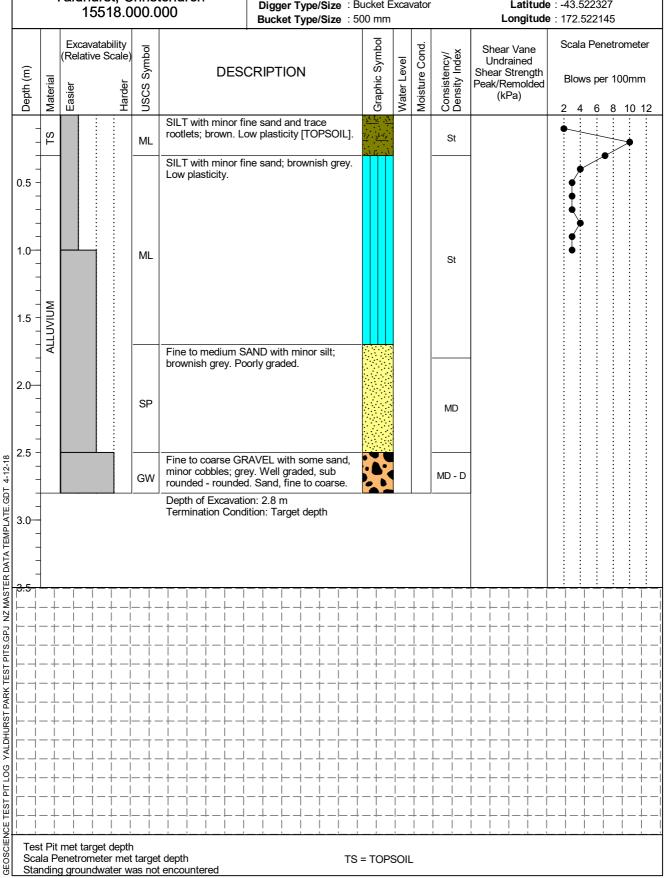




Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000

Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By : HB Date: 24/10/18 Reviewed By: HF

Max Test Pit Depth : 2.8 m

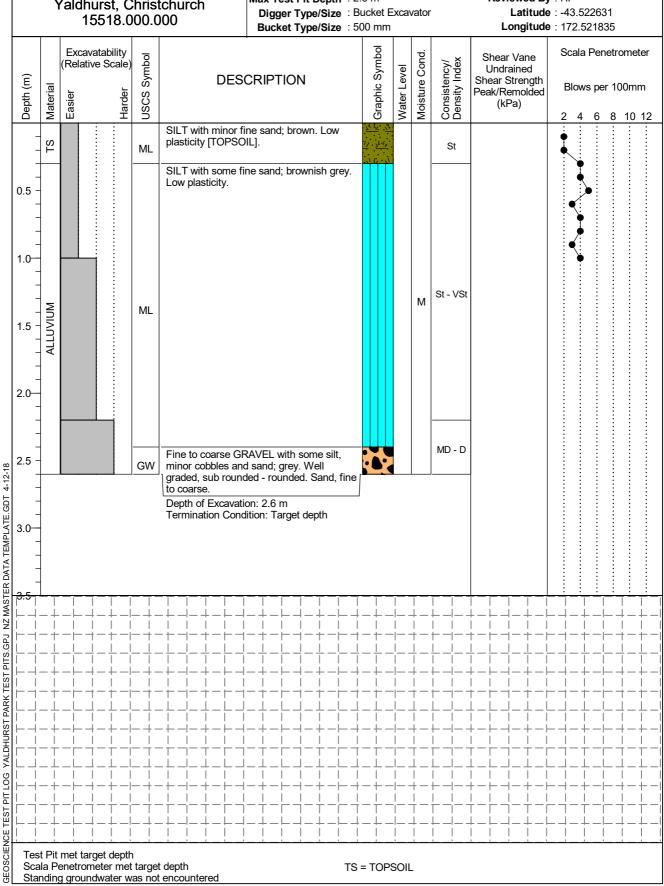




Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch

Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By : HB Date: 24/10/18 Reviewed By: HF

Max Test Pit Depth : 2.6 m



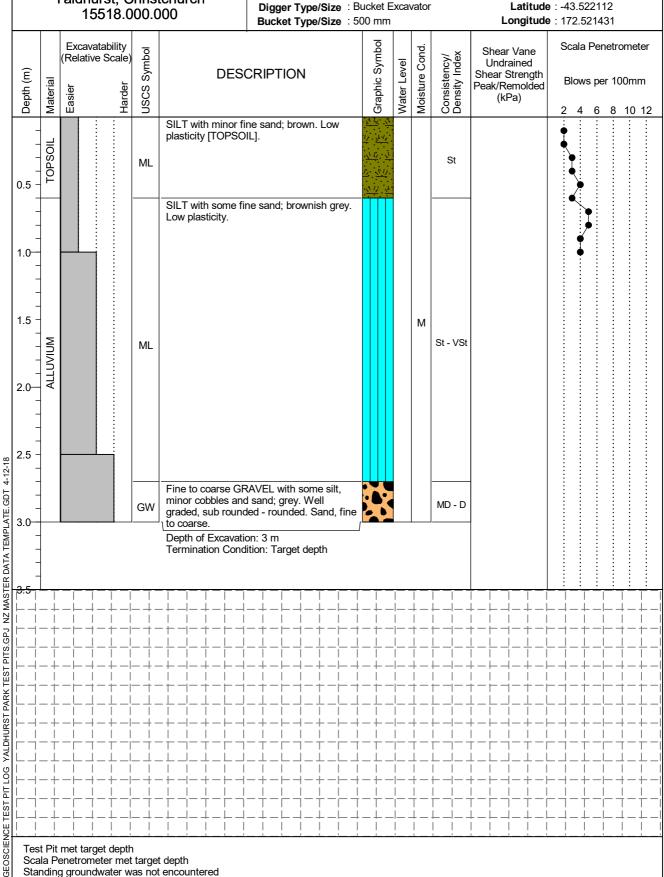


Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000

Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By : HB Date: 25/10/18 Reviewed By: HF

Max Test Pit Depth: 3 m

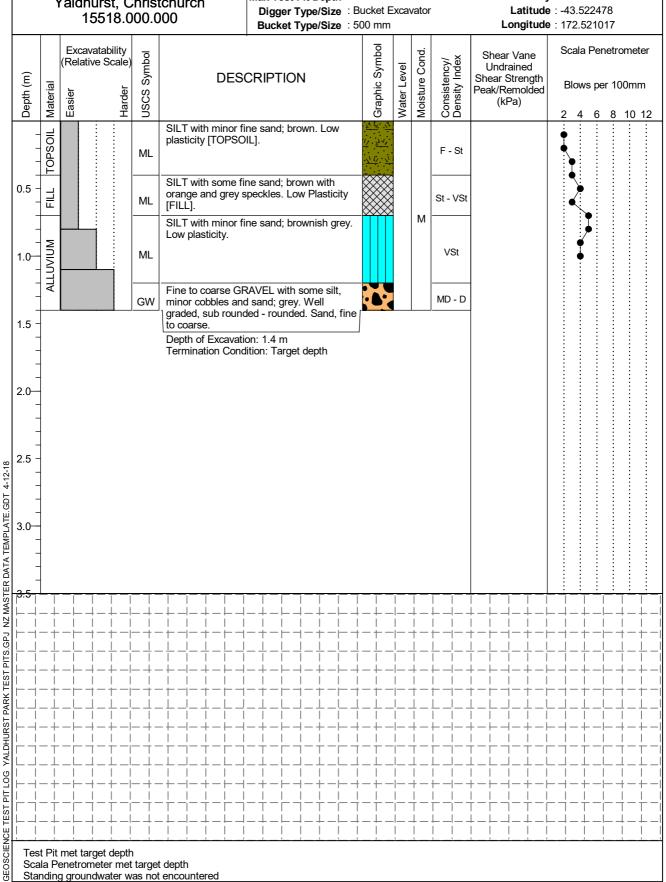
Digger Type/Size : Bucket Excavator Latitude : -43.522112 Longitude: 172.521431





Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch

Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By: HB Date: 25/10/18 Max Test Pit Depth: 1.4 m Reviewed By: HF

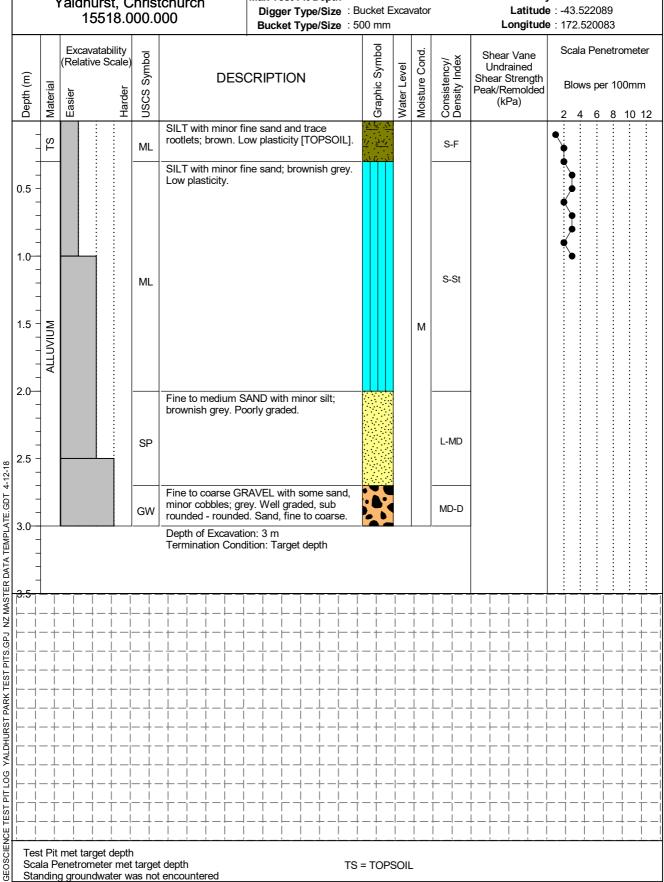




Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000

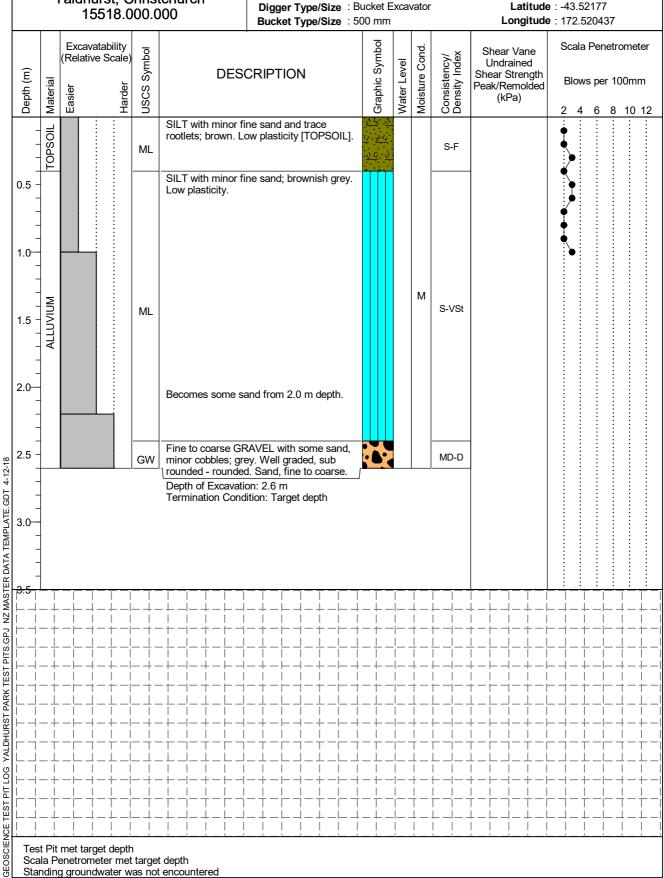
Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By: HB Date: 25/10/18 Reviewed By: HF

Max Test Pit Depth: 3 m



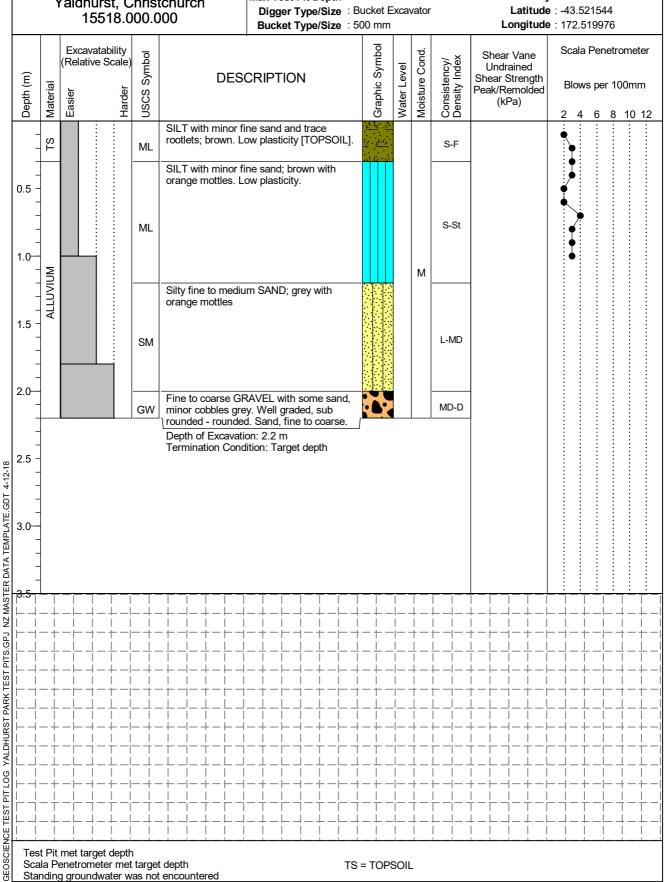


Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000 Max Test Pit Depth : 2.6 m Re
Digger Type/Size : Bucket Excavator





Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000 Max Test Pit Depth : 2.2 m

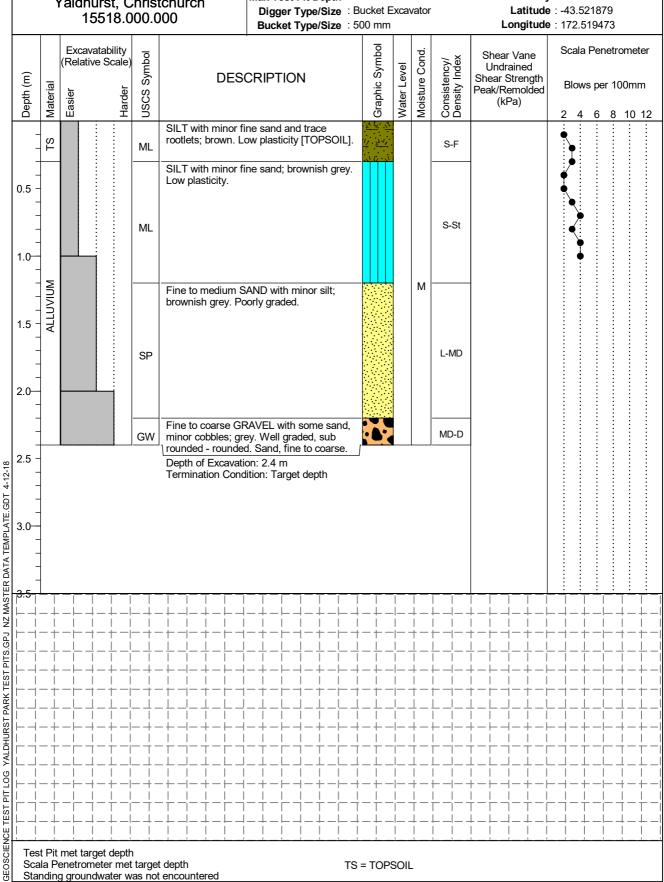




Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000 Client : Infinity Yaldhurst Limited Shear Vane No : NA

Date : 25/10/18 Logged By : HB

Max Test Pit Depth : 2.4 m Reviewed By : HF



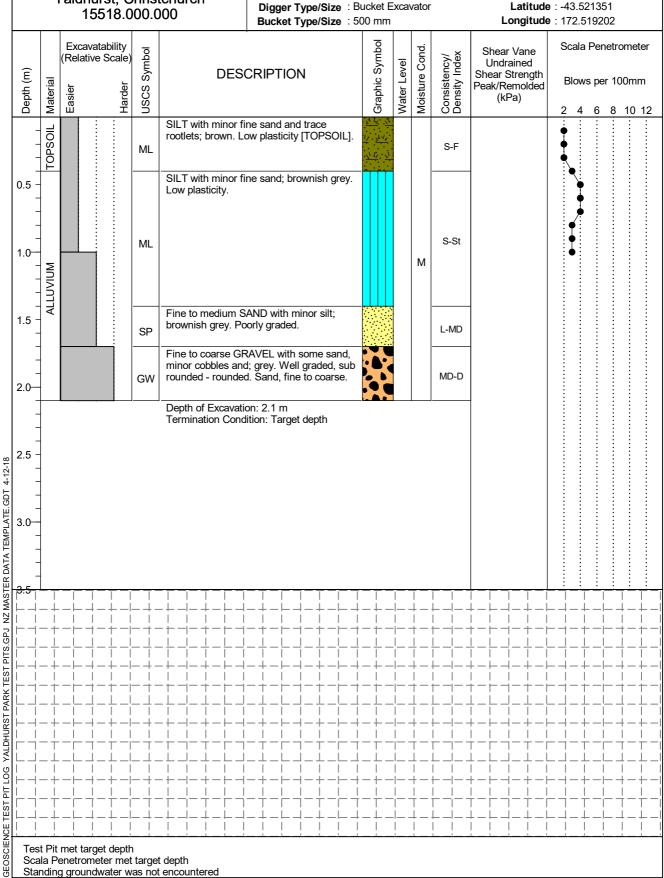


Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch

Shear Vane No: NA Client: Infinity Yaldhurst Limited Logged By: HB Date: 25/10/18

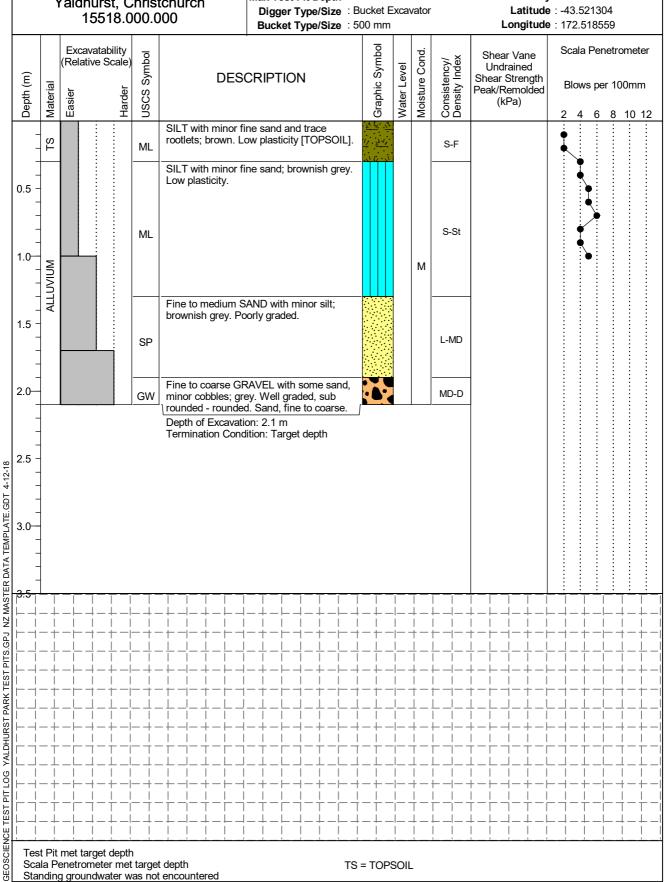
Max Test Pit Depth: 2.1 m Reviewed By: HF

Latitude: -43.521351





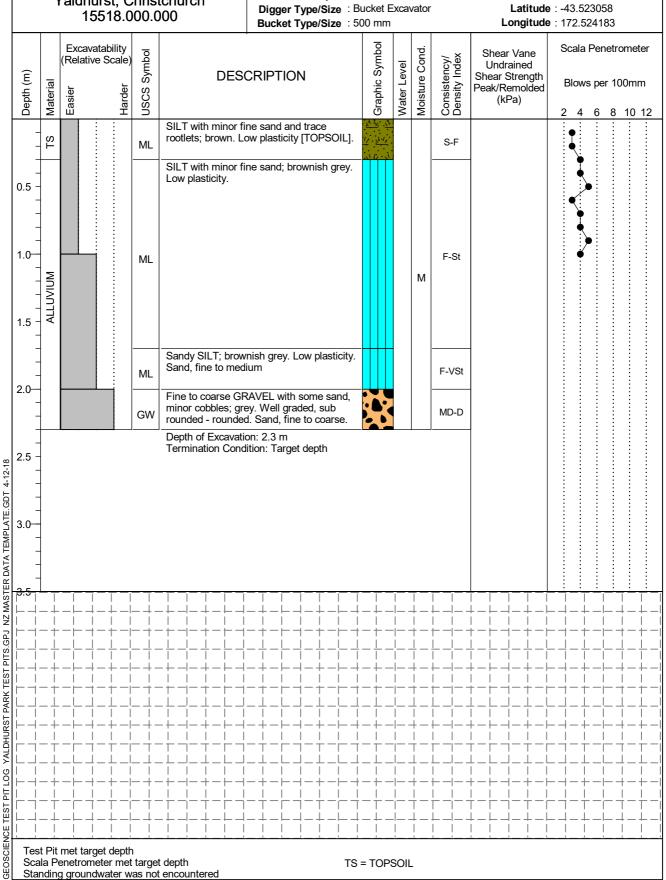
Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518 000 000 Max Test Pit Depth : 2.1 m Revie





Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000 Client: Infinity Yaldhurst Limited Shear Vane No: NA
Date: 25/10/18 Logged By: HB
Logged By: HB
Reviewed By: HF

Max Test Pit Depth : 2.3 m Reviewed By : HF



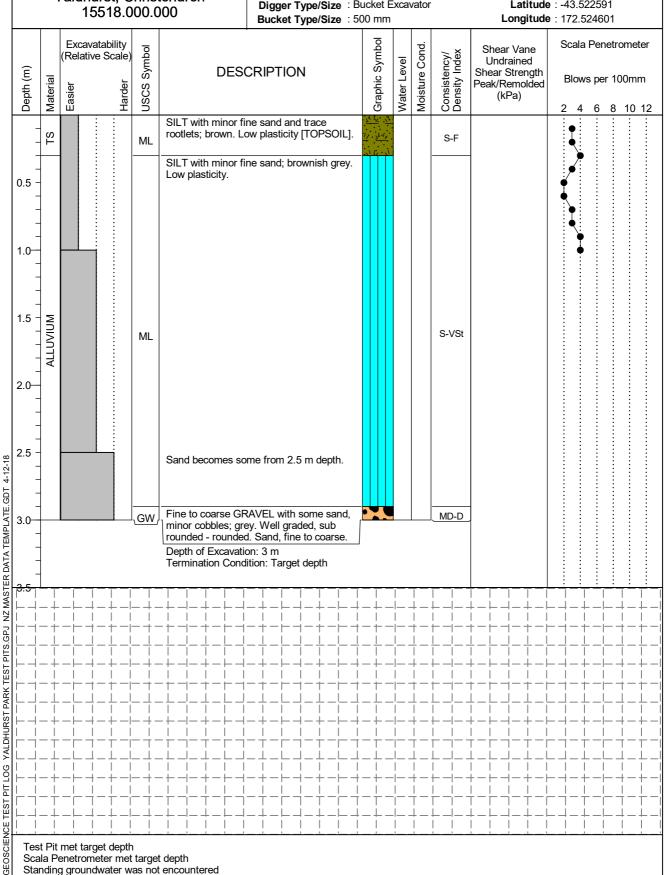


Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch

Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By: HB Date: 25/10/18

Max Test Pit Depth: 3 m Reviewed By: HF

Digger Type/Size : Bucket Excavator Latitude: -43.522591 Longitude: 172.524601

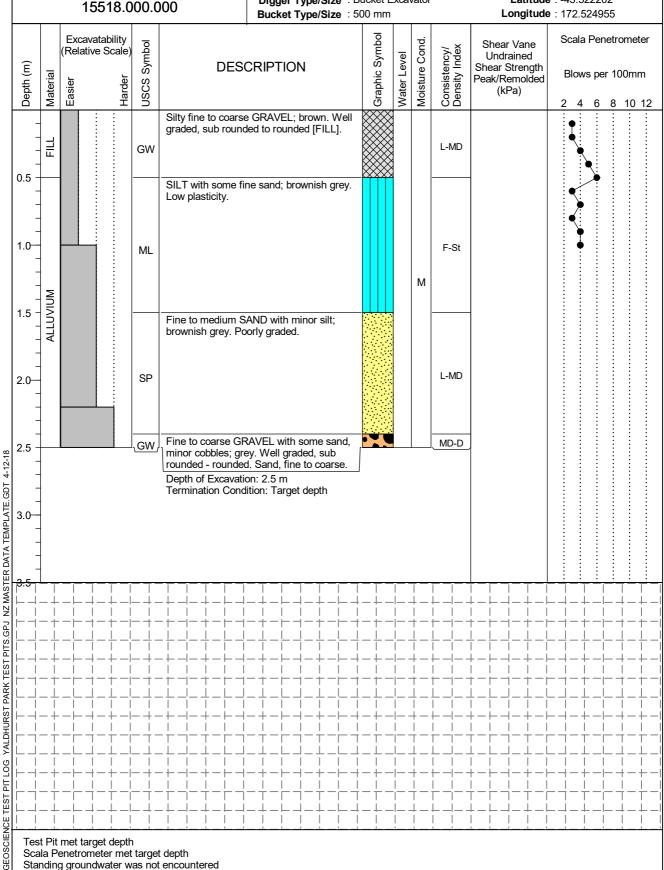




Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000

Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By: HB Date: 25/10/18 Reviewed By: HF

Max Test Pit Depth : 2.5 m

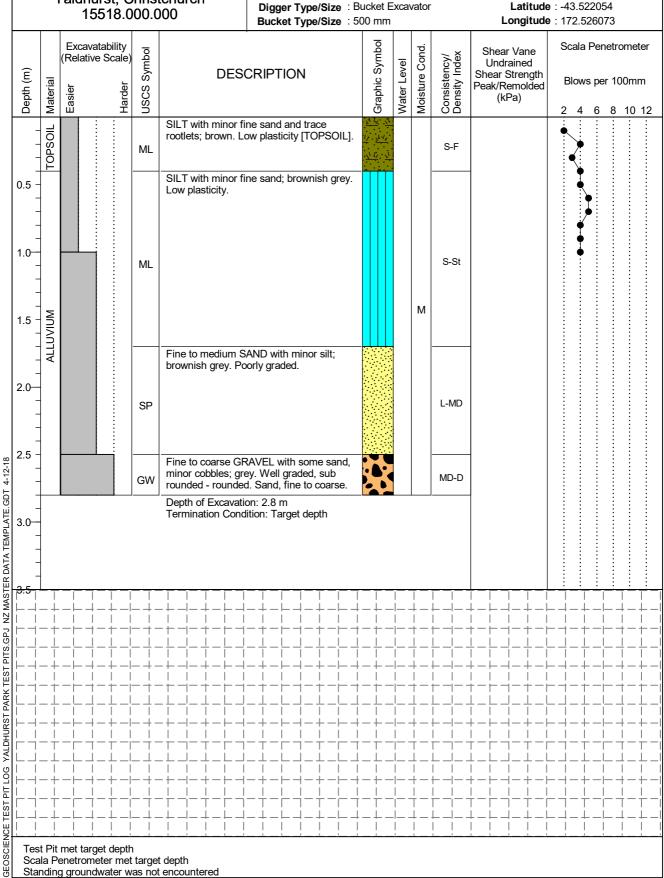




Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch

Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By: HB Date: 25/10/18 Reviewed By: HF

Max Test Pit Depth : 2.8 m



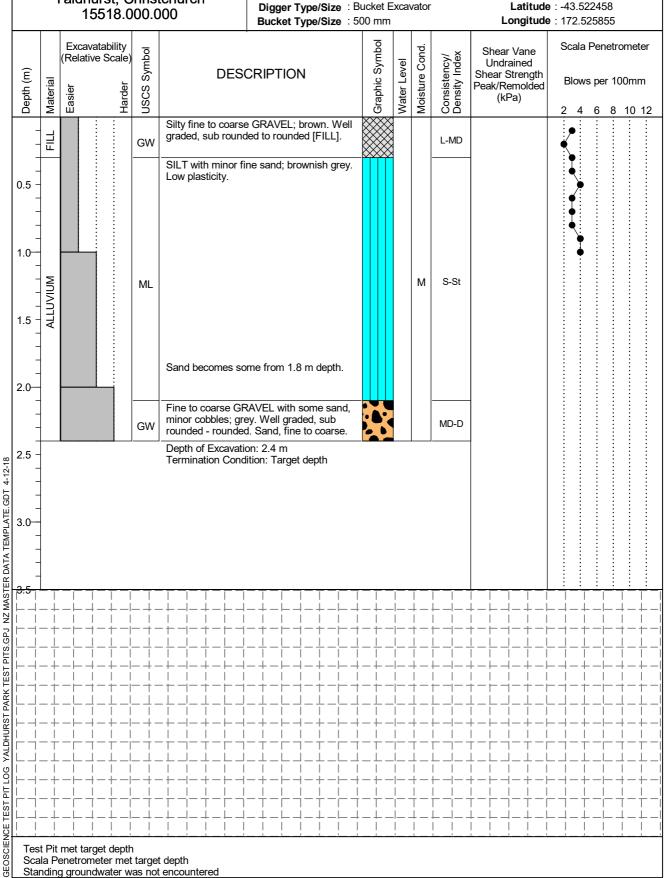


Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch

Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By: HB Date: 25/10/18 Reviewed By: HF

Max Test Pit Depth : 2.4 m

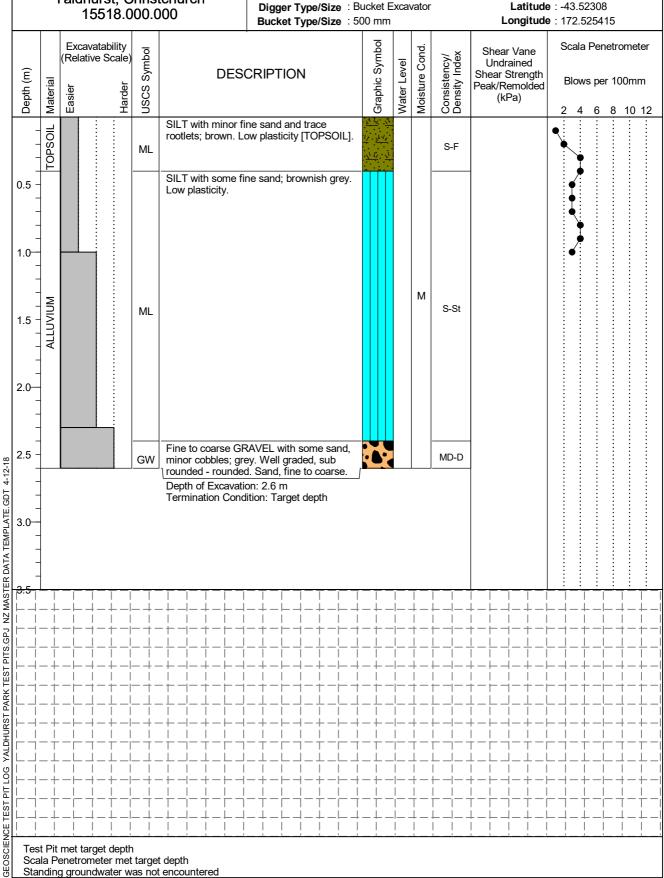
Latitude: -43.522458 Longitude: 172.525855





Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000 Client: Infinity Yaldhurst Limited
Date: 25/10/18
Logged By: HB
t Depth: 2.6 m
Reviewed By: HF

Max Test Pit Depth : 2.6 m Reviewed By : H
Digger Type/Size : Bucket Excavator Latitude : -4



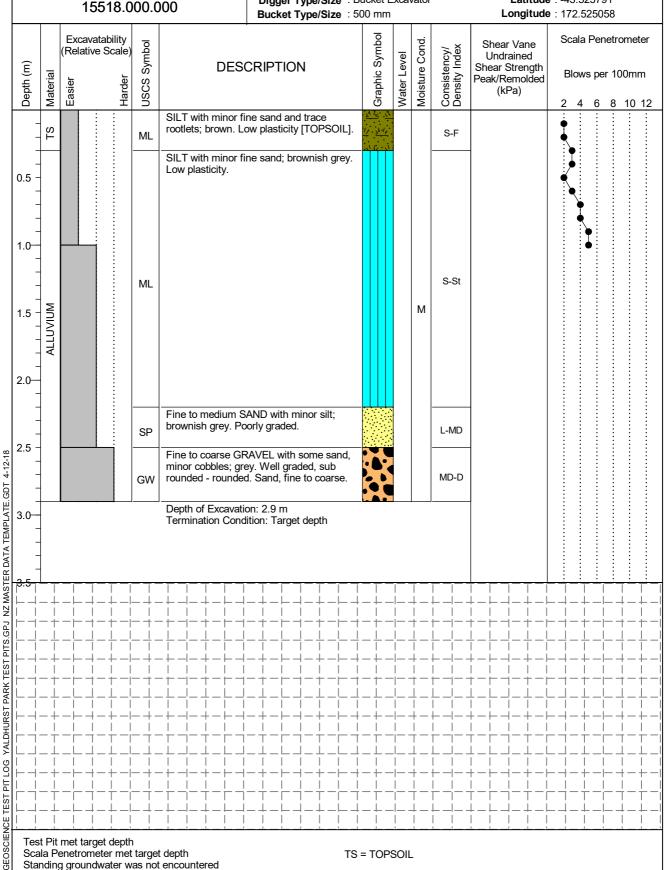


Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000

Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By: HB Date: 25/10/18 Max Test Pit Depth : 2.9 m Reviewed By: HF

Digger Type/Size : Bucket Excavator

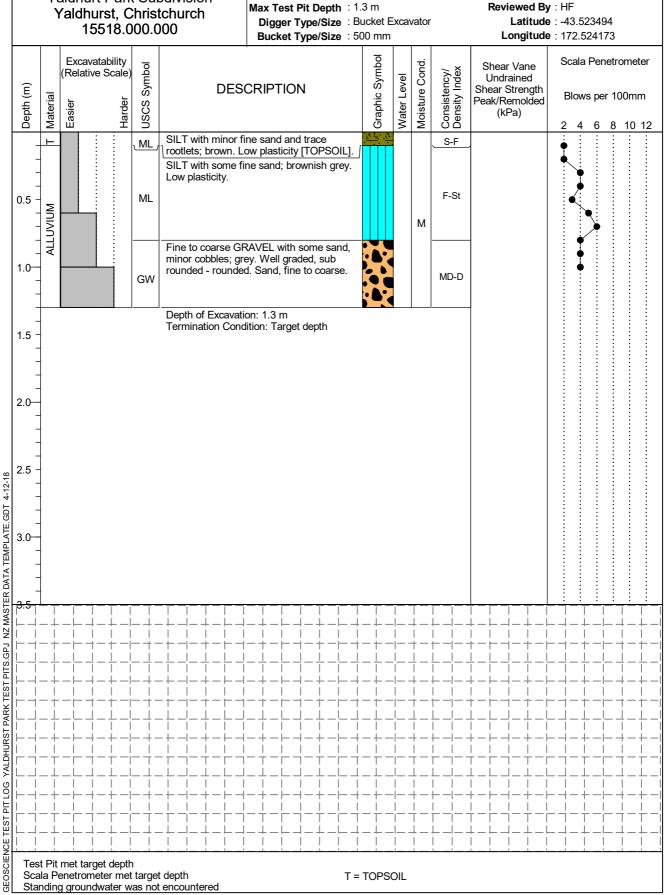
Latitude: -43.523791





Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch

Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By: HB Date : 26/10/18

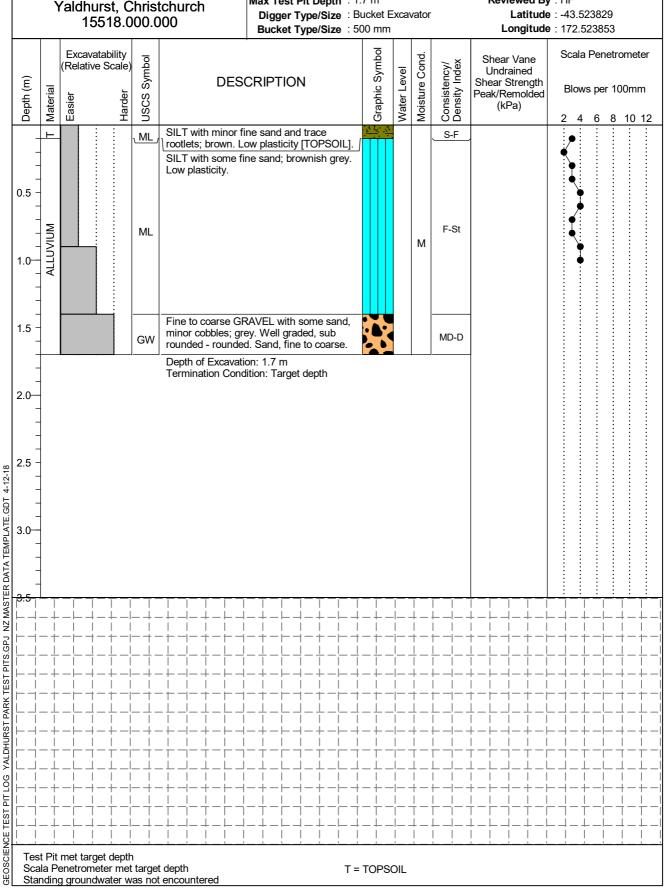




Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch

Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By: HB Date: 26/10/18 Reviewed By: HF

Max Test Pit Depth: 1.7 m



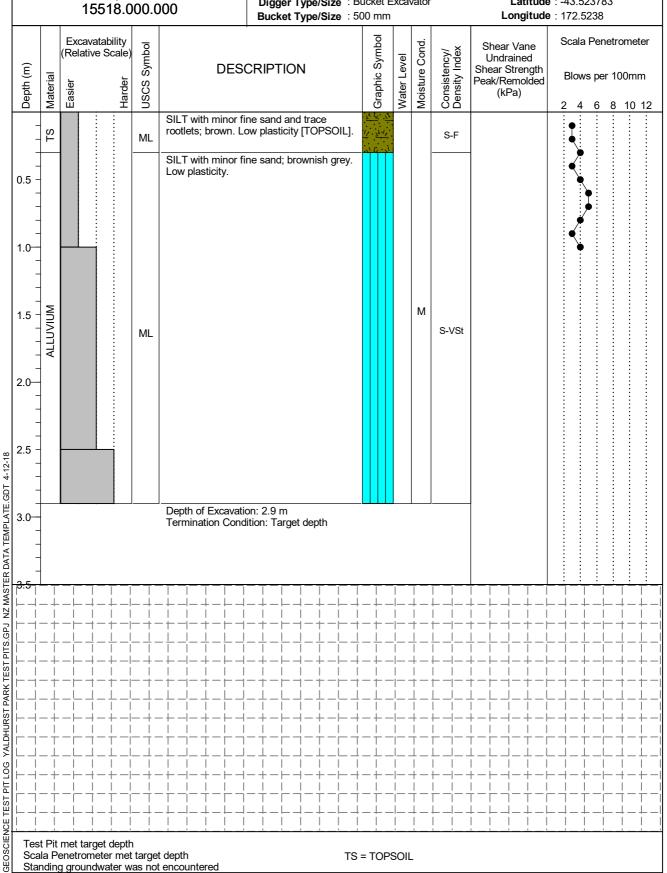


Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000

Client: Infinity Yaldhurst Limited Shear Vane No: NA Logged By: HB Date : 26/10/18

Max Test Pit Depth : 2.9 m Reviewed By: HF

Digger Type/Size : Bucket Excavator Latitude: -43.523783 Longitude: 172.5238





Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000 Client: Infinity Yaldhurst Limited

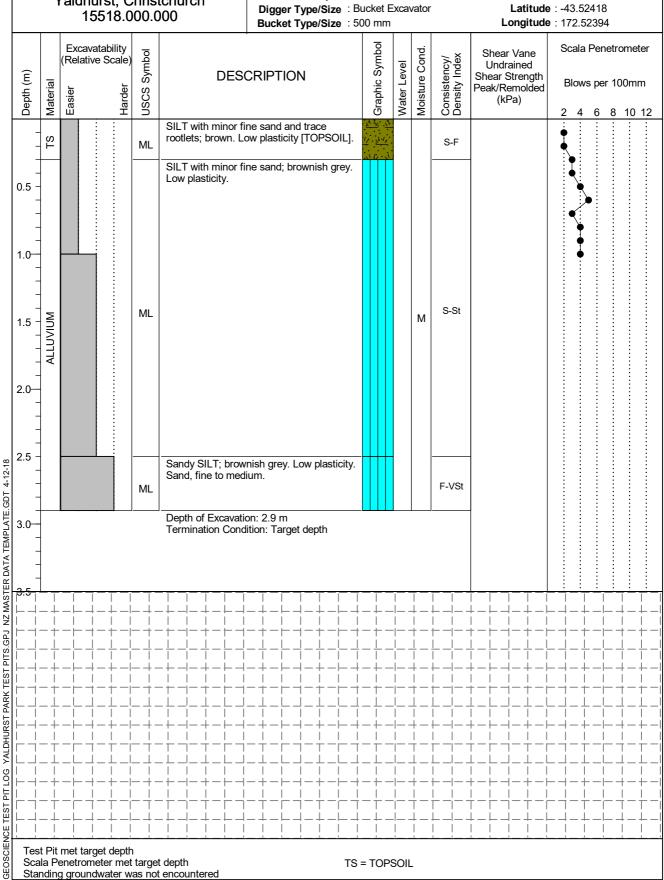
Date: 26/10/18

Logged By: HB

Depth: 2.9 m

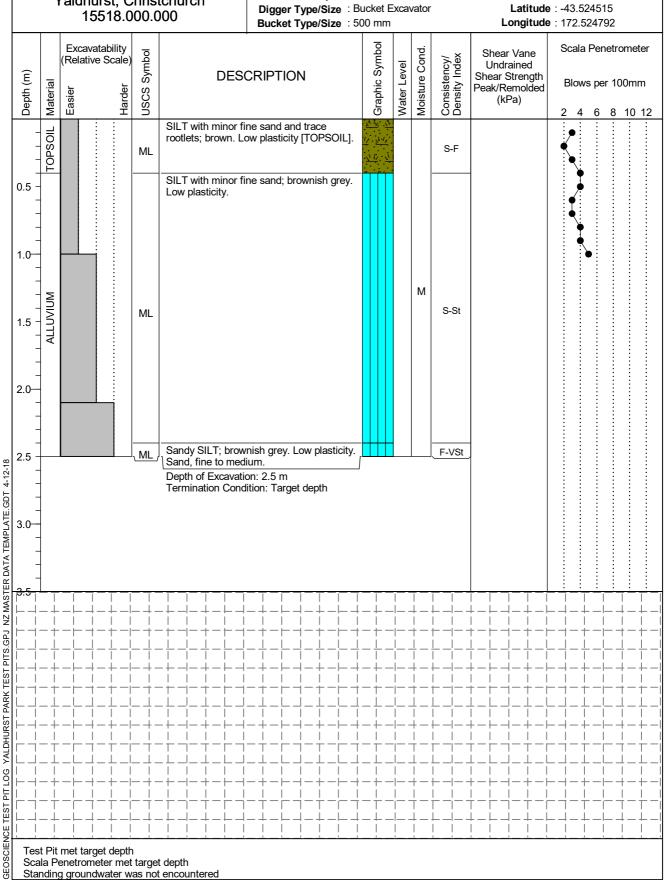
Reviewed By: HF

Max Test Pit Depth : 2.9 m Reviewed By : HF



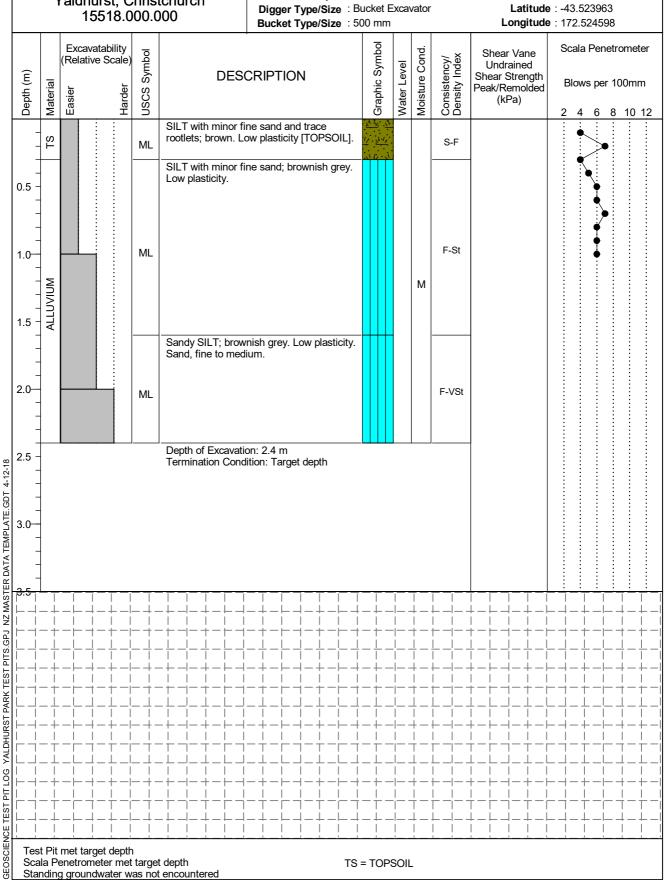


Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000 Max Test Pit Depth : 2.5 m





Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000 Max Test Pit Depth : 2.4 m Rev



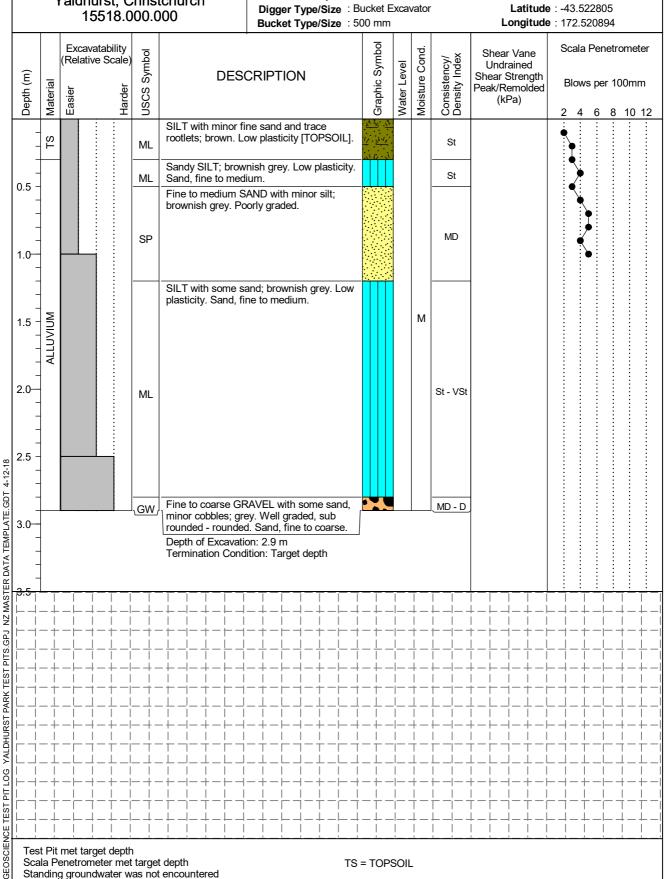


Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000 Client : Infinity Yaldhurst Limited Shear Vane No : NA

Date : 26/10/18 Logged By : HB

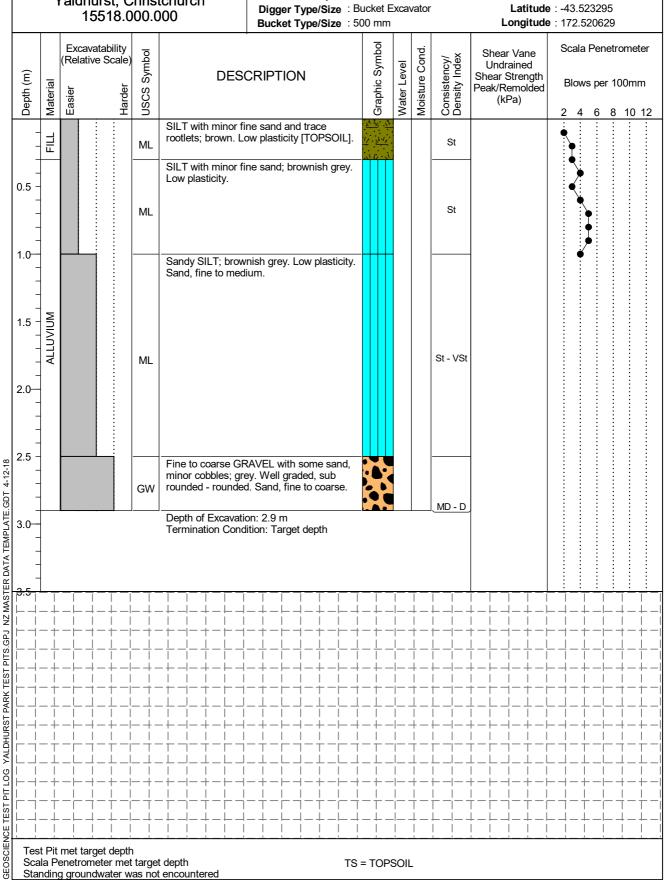
It Donth : 2.9 m Reviewed By : HE

Max Test Pit Depth : 2.9 m Reviewed By : HF





Yaldhurst Park Subdivision Yaldhurt Park Subdivision Yaldhurst, Christchurch 15518.000.000 Client: Infinity Yaldhurst Limited Date: 26/10/18 Shear Vane No: NA Logged By: HB
Max Test Pit Depth: 2.9 m Reviewed By: HF





APPENDIX 3:

Borehole Logs





Geotechnical Investigation Yaldhurst Park Yaldhurst, Christchurch 15518.000.000

Client: Infinity Yaldhurst Limited Core Diameter: 83 mm Date: 23/11/2018 Hammer Efficiency : 93.8~%Hole Depth: 10.89 m Logged By/Reviewed By : HF / DEB Drilling Method: Rotosonic Latitude: 172.519081

Drilling Contractor: McMillan Drilling Group Ltd Longitude: -43.521249

			100	318.000.000	Drilling Contract	tor : M	lcMil	llan I	Drilling	Group Ltd			ude : -43.5212	49
Depth (m)	Material	Sample Type	USCS Symbol	DESCRIPTIO	N	Log Symbol	Water Level	Moisture	Consistency/ Density Index	SPT N-Value	Pocket Pen. UCS (kPa)	Torvane Shear (kPa)	Total Core Recovery (%)	Note
-	TOPSOIL		ML	SILT with minor organics and trac brown. Low plasticity. Sand, fine	TOPSOIL].				S-F					
0.5 - - -			ML	SILT with trace sand; Yellowish b orange mottles. Low plasticity. Sa					F - VSt					
- 1.0-			SP	Silty fine SAND; yellowish brown mottles. Poorly graded.	with orange				L - MD					
			ML	Sandy SILT; Yellowish brown. Lo Sand, fine.	w plasticity.				F - VSt					
1.5		Ц	SP GP	Fine to medium SAND with trace brown. Poorly graded.					L - MD					
- - - 2.0—				Sandy fine to medium GRAVEL; Poorly graded, subangular to sub fine to medium.	brownish grey. rounded. Sand,					2,1,5,11,14,15 N=45				
- - -	/IUM							М						
2.5 - - - -	ALLUVIUM													
3.0— - -									MD - D	12,30,28,2 N=60+				
3.5 - -														
- 4.0 - - -														



Geotechnical Investigation Yaldhurst Park Yaldhurst, Christchurch

Client: Infinity Yaldhurst Limited Core Diameter: 83 mm Date: 23/11/2018 Hammer Efficiency : 93.8~% $\textbf{Hole Depth} : 10.89 \ m$ $\textbf{Logged By/Reviewed By} : \mathsf{HF} \ / \ \mathsf{DEB}$ Drilling Method: Rotosonic **Latitude**: 172.519081

			518.000.000	Drilling Contractor				Group Ltd			ude : -43.5212	49
Depth (m) Material	Sample Type	မှု USCS Symbol	DESCRIPTIO	DN &	Water Level	Moisture	Consistency/ Density Index	SPT N-Value	Pocket Pen. UCS (kPa)	Torvane Shear (kPa)	Total Core Recovery (%)	Note
5.0-		GP	Sandy fine to medium GRAVEL; Poorly graded, subangular to sub- fine to medium.	prounded. Sand,				1,13,17,15,12,1 N=60+				
5.5												
6.0				000				8,9,9,11,10,10 N=40				
6.5 - - - - - - - - - - - - - - - - - - -						М	MD - D					
7.5 -								20,40 N=60+				
8.0-												
8.5		SP	Fine to medium SAND with mind brownish grey. Poorly graded.	or gravel;			MD - D					



Geotechnical Investigation Yaldhurst Park Yaldhurst, Christchurch 15518.000.000

Drilling Contractor: McMillan Drilling Group Ltd Longitude: -43.521249

Depth (m)	Material	Sample Type	USCS Symbol	DESCRIPTION	Log Symbol	Water Level	Moisture	Consistency/ Density Index	SPT N-Value	Pocket Pen. UCS (kPa)	Torvane Shear (kPa)	Total Core Recovery (%)	Notes
9.5 -	AL		GW	Sandy fine to course GRAVEL; brownish grey. Well graded, subangular to subrounded. Sand, fine to coarse.			М	MD - D	16,24,27,31,2 N=60+ 16,24,27,31,2 N=60+				

End of Hole Depth: 10.89 m Termination: Target depth

Machine borehole met target depth at 10.89 m depth.

Standing groundwater was not encountered



Geotechnical Investigation Yaldhurst Park Yaldhurst, Christchurch 15518.000.000

Date: 23/11/2018 Hammer Efficiency: 96 % Hole Depth : 10.67 m

Drilling Method : Rotosonic Logged By/Reviewed By: HF / DEB

Latitude: 172.522091 Longitude: -43.523274

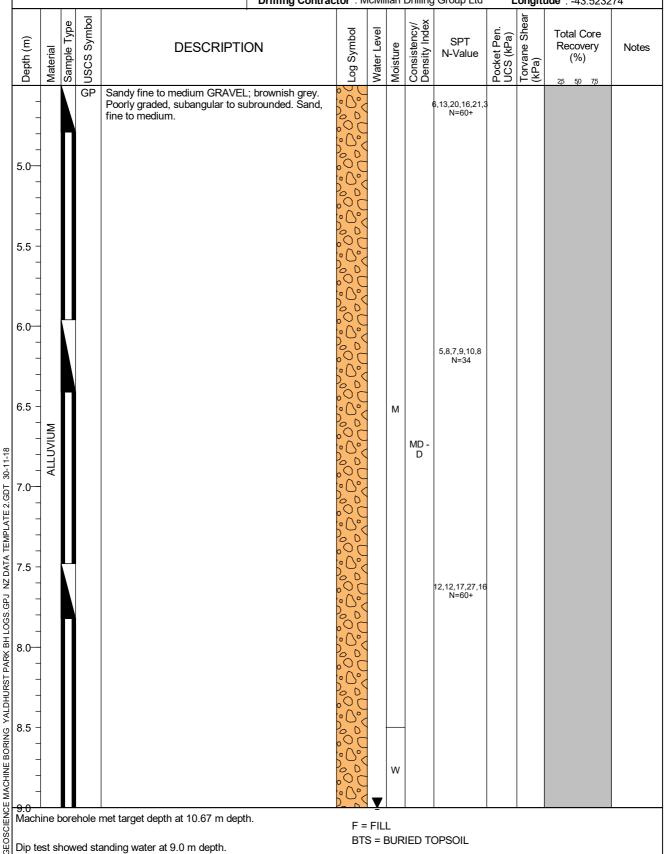
			15	Drilling Contr	actor : N	1cMi	llan	Drilling	Group Ltd			ude:-43.5232	74
Depth (m)	Material	Sample Type	USCS Symbol	DESCRIPTION	Log Symbol	Water Level	Moisture	Consistency/ Density Index	SPT N-Value	Pocket Pen. UCS (kPa)	Torvane Shear (kPa)	Total Core Recovery (%)	Notes
-	ш		GW	Sandy GRAVEL with trace silt and organics; greyish brown. Well graded. Sand, fine to coarse [FILL].				L					
-	BTS		ML	SILT with some sand and trace organics; dark brown. Low plasticity. Sand, fine [BTS].	17.31.			S-F					
0.5 -			SP	Silty fine SAND; yellowish brown with orange mottles. Poorly graded.									
1.0-								L - MD					
1.5 -			ML	SILT with minor sand; Yellowish brown. Low plasticity. Sand, fine.				F - St	3,3,3,3,4,5 N=15				
- -		A	SP	Silty fine SAND; yellowish brown with orange mottles. Poorly graded.					14-15				
2.0— - - 2.5 - - - - 3.0—	MD						М	L - MD					
2.5 -	ALLUVIUM			Becomes SAND with some silt from 2.5 m depth									
	-		GP	Sandy fine to medium GRAVEL; brownish grey. Poorly graded, subangular to subrounded. Sand, fine to medium.					7,9,12,21,27 N=60+				
3.5 -	-							MD - D					
3.5	-												
4.5 Mach				met target depth at 10.67 m depth.		FIL		IFD T	OPSOIL	1	1		
Dip to	est sl	how	ed sta	anding water at 9.0 m depth.	יוט				E				

Geotechnical Investigation Yaldhurst Park Yaldhurst, Christchurch 15518.000.000

Dip test showed standing water at 9.0 m depth.

Client: Infinity Yaldhurst Limited Core Diameter: 83 mm Date: 23/11/2018 Hammer Efficiency : 96 %Hole Depth: 10.67 m $\textbf{Logged By/Reviewed By} : \mathsf{HF} \ / \ \mathsf{DEB}$ Drilling Method: Rotosonic Latitude: 172.522091

Drilling Contractor: McMillan Drilling Group Ltd Longitude: -43.523274



BTS = BURIED TOPSOIL



Geotechnical Investigation Yaldhurst Park Yaldhurst, Christchurch 15518.000.000 Client : Infinity Yaldhurst Limited Core Diameter : 83 mm

Date : 23/11/2018 Hammer Efficiency : 96 %

Hole Depth : 10.67 m Logged By/Reviewed By : HF / DEB

Drilling Method : Rotosonic Latitude : 172.522091

Drilling Contractor: McMillan Drilling Group Ltd Longitude: -43.523274

Depth (m)	Material	Sample Type	USCS Symbol	DESCRIPTION	Log Symbol	Water Level	Moisture	Consistency/ Density Index	SPT N-Value	Pocket Pen. UCS (kPa)	Torvane Shear (kPa)	Total Core Recovery (%)	Notes
9.5 -	М		GP ML	Sandy fine to medium GRAVEL; brownish grey. Poorly graded, subangular to subrounded. Sand, fine to medium. SILT with trace gravel and clay; yellowish brown. Low plasticity.				MD - D	22,38 N=60+				
10. 0 10.5	ALLUVIUM		GW	Sandy fine to course GRAVEL; brownish grey. Well graded, subangular to subrounded. Sand, fine to coarse.			S	MD -	15,45 N=60+				

End of Hole Depth: 10.67 m Termination: Target depth

LOG OF BORING BH03 Client: Infinity Yaldhurst Limited Core Diameter: 83 mm Geotechnical Investigation Date: 23/11/2018 Hammer Efficiency : 96 %Yaldhurst Park Hole Depth: 10.8 m $\textbf{Logged By/Reviewed By} : \mathsf{HF} \ / \ \mathsf{DEB}$ Yaldhurst, Christchurch Drilling Method: Rotosonic $\textbf{Latitude}\ : 172.524153$ 15518.000.000 **Drilling Contractor**: McMillan Drilling Group Ltd **Longitude**: -43.523375 Torvane Shear (kPa) **USCS Symbol** Consistency/ Density Index Sample Type Pocket Pen. UCS (kPa) Log Symbol Water Level **Total Core** Depth (m) SPT Recovery **DESCRIPTION** Moisture Notes Material N-Value (%) SILT with trace organics and sand; brown. Low S-F plasticity. Sand, fine [TOPSOIL]. SILT with trace sand; Yellowish brown with orange mottles. Low plasticity. Sand, fine. S - St 0.5 Sandy fine to medium GRAVEL; brownish grey. Poorly graded, subangular to subrounded. Sand, GP fine to medium. 1.0 1.5 10,12,10,8,10,14 2.0 Μ GEOSCIENCE MACHINE BORING YALDHURST PARK BH LOGS, GPJ NZ DATA TEMPLATE 2.GDT 30-11-18 2.5 MD3.0 17,27,40,20 N=60+ 3.5 Machine borehole met target depth at 10.8 m depth.

T = TOPSOIL

Dip test showed standing water at 7.5 m depth.



Geotechnical Investigation Yaldhurst Park Yaldhurst, Christchurch 15518.000.000

Dip test showed standing water at 7.5 m depth.

Date: 23/11/2018 Hammer Efficiency: 96 % Hole Depth: 10.8 m Logged By/Reviewed By: HF / DEB
Drilling Method: Rotosonic Latitude: 172.52415

Latitude: 172.524153 Longitude: -43.523375

			15	518.000.000	Drilling Contract	ctor : M	lcMi	lan	Drilling	Group Ltd	L		ude : -43.5233	75
Depth (m)	Material	Sample Type	USCS Symbol	DESCRIPTION		Log Symbol	Water Level	Moisture	Consistency/ Density Index	SPT N-Value	Pocket Pen. UCS (kPa)	Torvane Shear (kPa)	Total Core Recovery (%)	Notes
5.0			GP	Sandy fine to medium GRAVEL Poorly graded, subangular to su fine to medium.	.; brownish grey. Ibrounded. Sand,				MD - D	20,26,30,30 N=60+				
6.0			SW	Gravelly fine to coarse SAND; bgraded.	orownish grey. Well			M	MD - D					
6.5 -	ALLUVIUM		GP	Sandy fine to medium GRAVEL brownish grey. Poorly graded, s subrounded. Sand, fine to medi	with trace silt; ubangular to um.					20,17,13,7,8,8 N=36				
7.0 - - - 7.5 - -							▼.	W	MD - D	11,15,13,10,8,6 N=37	3			
8.0 - - - 8.5 -								S						
9.0 Mach	ine b	oore	ehole :	met target depth at 10.8 m depth										

T = TOPSOIL



Geotechnical Investigation Yaldhurst Park Yaldhurst, Christchurch 15518.000.000 Client: Infinity Yaldhurst Limited Core Diameter: 83 mm

Date: 23/11/2018 Hammer Efficiency: 96 %

Hole Depth: 10.8 m Logged By/Reviewed By: HF / DEB

Drilling Method: Rotosonic Latitude: 172.524153

Drilling Contractor: McMillan Drilling Group Ltd **Longitude**: -43.523375

Depth (m)	Material	Sample Type	USCS Symbol	DESCRIPTION	Log Symbol	Water Level	Moisture	Consistency/ Density Index	SPT N-Value	Pocket Pen. UCS (kPa)	Torvane Shear (kPa)	Total Core Recovery (%)	Notes
9.5 -	A		GP	Sandy fine to medium GRAVEL with trace silt; brownish grey. Poorly graded, subangular to subrounded. Sand, fine to medium.			S	MD - D	11,9,9,8,8,7 N=32 15,29,30,30 N=60+				

End of Hole Depth: 10.8 m Termination: Target depth



Geotechnical Investigation Yaldhurst Park Yaldhurst, Christchurch 15518.000.000

Client: Infinity Yaldhurst Limited Core Diameter: 83 mm Date: 23/11/2018 Hammer Efficiency : 93.8~%Hole Depth: 10.91 m $\textbf{Logged By/Reviewed By} : \mathsf{HF} \ / \ \mathsf{DEB}$ **Drilling Method**: Rotosonic **Latitude**: 172.523697

Drilling Contractor: McMillan Drilling Group Ltd **Longitude**: -43.521794

Sample Type	USCS Symbol	DESCRIPTIO		loc	/el		cy/ dex		(hear	Total Core	
: ഗ	USC	BESON TO	ON	Log Symbol	Water Level	Moisture	Consistency/ Density Index	SPT N-Value	Pocket Pen. UCS (kPa)	Torvane S (kPa)	Recovery (%)	Notes
	ML	SILT with trace organics and sa Low plasticity. Sand, fine [TOPS	nd; dark brown. SOIL].	17 - 34 19 - 34 17 - 34 19 - 34 19 - 34 19 - 34 19 - 34 19 - 34 19 19 19 19 19 19 19 19 19 19 19 19 19			S-F					
	ML	SILT with some sand; Yellowish orange mottles. Low plasticity. §	brown with Sand, fine.				F - St					
	SP	Silty fine SAND; yellowish brown mottles. Poorly graded.	n with orange				L - MD					
	ML	SILT with trace sand; Yellowish plasticity. Sand, fine.	brown. Low				F - St					
	GP	Sandy fine to medium GRAVEL Poorly graded, subangular to su fine to medium.	; brownish grey. brounded. Sand,				(5,9,10,14,14,22 N=60+				
						М						
							MD - D	14,20,23,23,14 N=60+				
		ML SP	ML SILT with some sand; Yellowish orange mottles. Low plasticity. Silty fine SAND; yellowish brown mottles. Poorly graded. ML SILT with trace sand; Yellowish plasticity. Sand, fine. GP Sandy fine to medium GRAVEL Poorly graded, subangular to su fine to medium.	ML SILT with some sand; Yellowish brown with orange mottles. Low plasticity. Sand, fine. SP Silty fine SAND; yellowish brown with orange mottles. Poorly graded. ML SILT with trace sand; Yellowish brown. Low plasticity. Sand, fine. GP Sandy fine to medium GRAVEL; brownish grey. Poorly graded, subangular to subrounded. Sand, fine to medium.	ML SILT with some sand; Yellowish brown with orange mottles. Low plasticity. Sand, fine. SP Silty fine SAND; yellowish brown with orange mottles. Poorly graded. ML SILT with trace sand; Yellowish brown. Low plasticity. Sand, fine. GP Sandy fine to medium GRAVEL; brownish grey. Poorly graded, subangular to subrounded. Sand, fine to medium.	ML SILT with some sand; Yellowish brown with orange mottles. Low plasticity. Sand, fine. SP Silty fine SAND; yellowish brown with orange mottles. Poorly graded. ML SILT with trace sand; Yellowish brown. Low plasticity. Sand, fine. GP Sandy fine to medium GRAVEL; brownish grey. Poorly graded, subangular to subrounded. Sand, fine to medium.	ML SILT with some sand; Yellowish brown with orange mottles. Low plasticity. Sand, fine. SP Sity fine SAND; yellowish brown with orange mottles. Poorly graded. ML SILT with trace sand; Yellowish brown. Low plasticity. Sand, fine. GP Sandy fine to medium GRAVEL; brownish grey. Poorly graded, subangular to subrounded. Sand, fine to medium.	ML SILT with some sand; Yellowish brown with orange mottles. Low plasticity. Sand, fine. SP Silty fine SAND; yellowish brown with orange mottles. Poorly graded. L - MD ML SILT with trace sand; Yellowish brown. Low plasticity. Sand, fine. GP Sandy fine to medium GRAVEL; brownish grey. Poorly graded, subangular to subrounded. Sand, fine to medium.	ML SILT with some sand; Yellowish brown with orange mottles. Low plasticity. Sand, fine. SP Silty fine SAND; yellowish brown with orange mottles. Poorly graded. L - MD ML SILT with trace sand; Yellowish brown. Low plasticity. Sand, fine. GP Sandy fine to medium GRAVEL; brownish grey. Poorly graded, subangular to subrounded. Sand, fine to medium. MM M MD - D 14.20,23,23,14 N=60+	ML SILT with some sand; Yellowish brown with orange mottles. Low plasticity. Sand, fine. SP Sity fine SAND; yellowish brown with orange mottles. Poorly graded. L - MD ML SILT with trace sand; Yellowish brown. Low plasticity. Sand, fine. GP Sandy fine to medium GRAVEL; brownish grey. Poorly graded, subangular to subrounded. Sand, fine to medium. MM M MD - D 14,20,23,23,14	ML SILT with some sand; Yellowish brown with orange mottles. Low plasticity. Sand, fine. SP Silty fine SAND; yellowish brown with orange mottles. Poorly graded. L - MD ML SILT with trace sand; Yellowish brown. Low plasticity. Sand, fine. GP Sandy fine to medium GRAVEL; brownish grey, Poorly graded, subangular to subrounded. Sand, fine to medium. MM MD D D D D D D D D D D D D D D D D	ML SILT with some sand; Yellowish brown with orange mottles. Low plasticity. Sand, fine. SP Silty fine SAND; yellowish brown with orange mottles. Poorly graded. L - MD ML SILT with trace sand; Yellowish brown. Low plasticity. Sand, fine. GP Sandy fine to medium GRAVEL; brownish grey, Poorly graded, subangular to subrounded. Sand, fine to medium. M M M M M M M M M M M M M M M



Geotechnical Investigation Yaldhurst Park Yaldhurst, Christchurch 15518.000.000 Client: Infinity Yaldhurst Limited Core Diameter: 83 mm

Date: 23/11/2018 Hammer Efficiency: 93.8 %

Hole Depth: 10.91 m Logged By/Reviewed By: HF / DEB

Drilling Method: Rotosonic Latitude: 172.523697

Drilling Contractor: McMillan Drilling Group Ltd Longitude: -43.521794

	150	518.000.000	Drilling Contract	tor : M	cMil	lan [Drilling	Group Ltd			ude: -43.5217	94
Depth (m) Material	Sample Type USCS Symbol	DESCRIPTIO		Log Symbol	Water Level	Moisture	Consistency/ Density Index	SPT N-Value	Pocket Pen. UCS (kPa)	Torvane Shear (kPa)	Total Core Recovery (%)	Notes
5.0-	GP	Sandy fine to medium GRAVEL Poorly graded, subangular to su fine to medium.	hrounded Sand					17,15,20,20,20 N=60+				
5.5												
6.5 - WILLUMAN ALL						М	1 MD - D	0,10,10,13,11, N=39	5			
7.5 -							8	,13,11,11,13,1 N=52	7			
8.5		met target depth at 10.91 m depth										



Geotechnical Investigation Yaldhurst Park Yaldhurst, Christchurch 15518.000.000 Client: Infinity Yaldhurst Limited Core Diameter: 83 mm

Date: 23/11/2018 Hammer Efficiency: 93.8 %

Hole Depth: 10.91 m Logged By/Reviewed By: HF / DEB

Drilling Method: Rotosonic Latitude: 172.523697

Drilling Contractor: McMillan Drilling Group Ltd Longitude: -43.521794

Depth (m)	Material	Sample Type	USCS Symbol	DESCRIPTION	Log Symbol	Water Level	Moisture	Consistency/ Density Index	SPT N-Value	Pocket Pen. UCS (kPa)	Torvane Shear (kPa)	Total Core Recovery (%)	Notes
9.5 -	ALLUVIUM		GP				М	MD - D	17.22,30,30 N=60+				

End of Hole Depth: 10.91 m Termination: Target depth

Machine borehole met target depth at 10.91 m depth.

Standing groundwater was not encountered



APPENDIX 4:

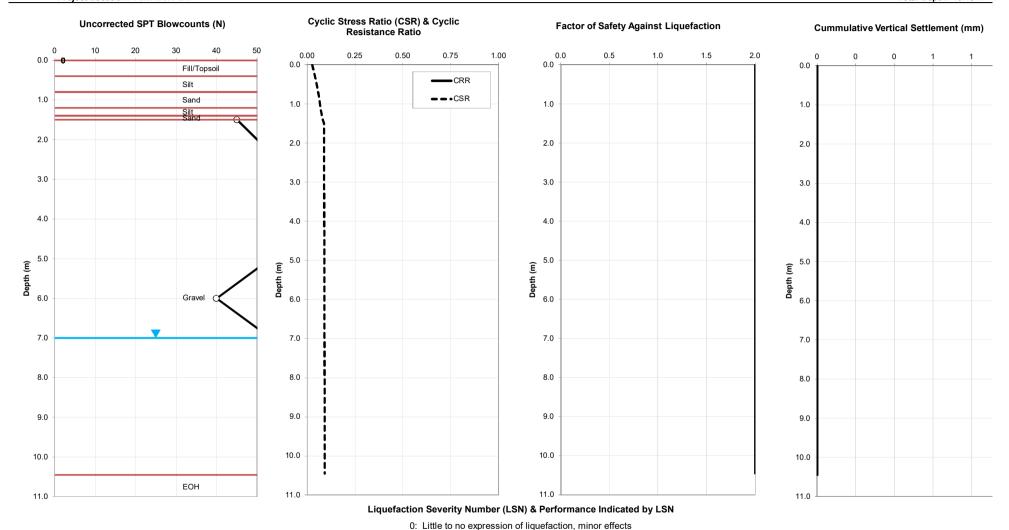
Liquefaction Analysis



Project Name: Subdivision Development

Project Location: Yaldhurst Park

Total Depth: 10.45 m



ENGEO Ref: 15518.000.000 Author: HF Reviewer: DEB Date: 1/12/2018 Design Case: SLS Case 1 Magnitude: 7.5 PGA (g): 0.13

Analysis Method: Idriss and Boulanger (2008,2010)

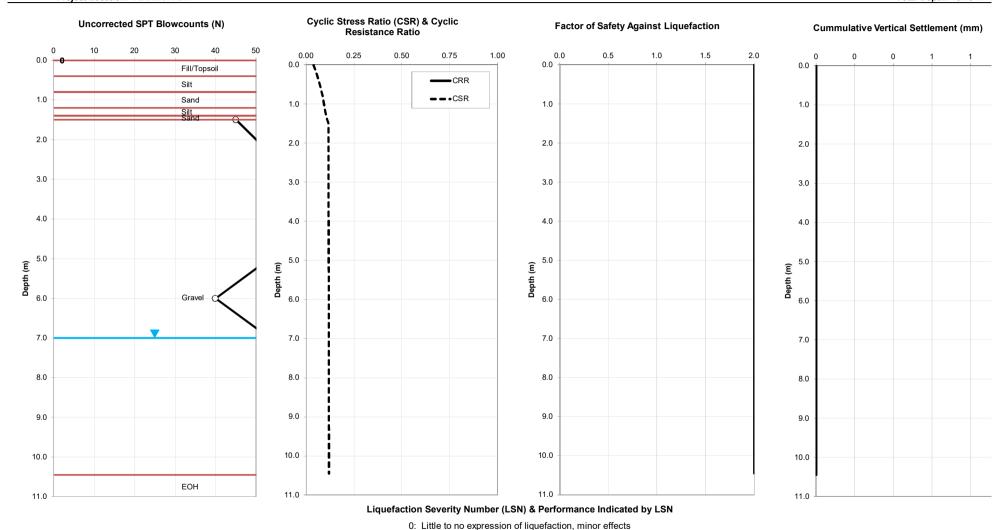
Groundwater Depth (m): 7
Probability of Liquefaction Curve Used: 16 %

Vertical Settlement Method: Ishihara & Yoshimine (1992)

Project Name: Subdivision Development

Project Location: Yaldhurst Park

Total Depth: 10.45 m



ENGEO Ref: 15518.000.000 Author: HF Reviewer: DEB Date: 1/12/2018 Design Case: SLS Case 2 Magnitude: 6 PGA (g): 0.19

Analysis Method: Idriss and Boulanger (2008,2010)

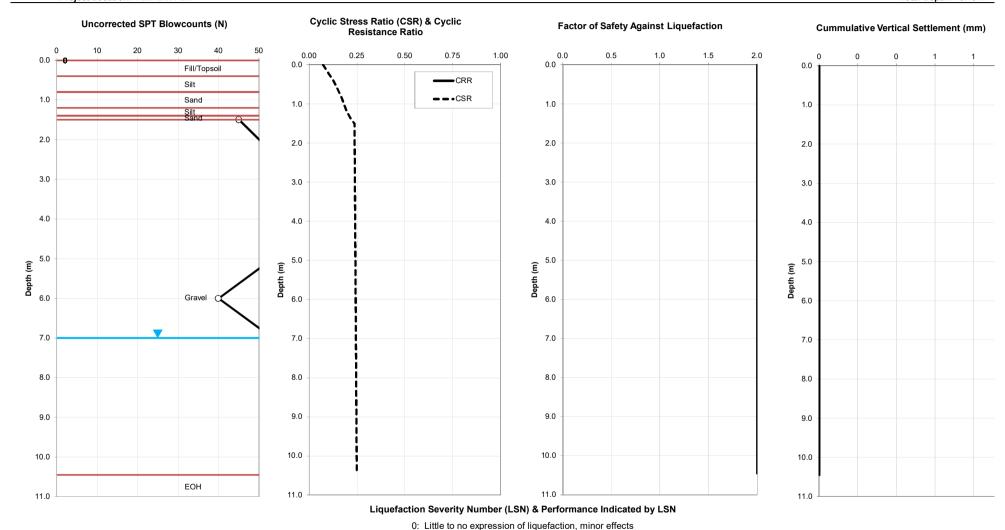
Groundwater Depth (m): 7
Probability of Liquefaction Curve Used: 16 %

Vertical Settlement Method: Ishihara & Yoshimine (1992)

Project Name: Subdivision Development

Project Location: Yaldhurst Park

Total Depth: 10.45 m



ENGEO Ref: 15518.000.000 Author: HF

Reviewer: DEB Date: 1/12/2018 Design Case: ULS Magnitude: 7.5 PGA (g): 0.35

Analysis Method: Idriss and Boulanger (2008,2010)

Groundwater Depth (m): 7
Probability of Liquefaction Curve Used: 16 %

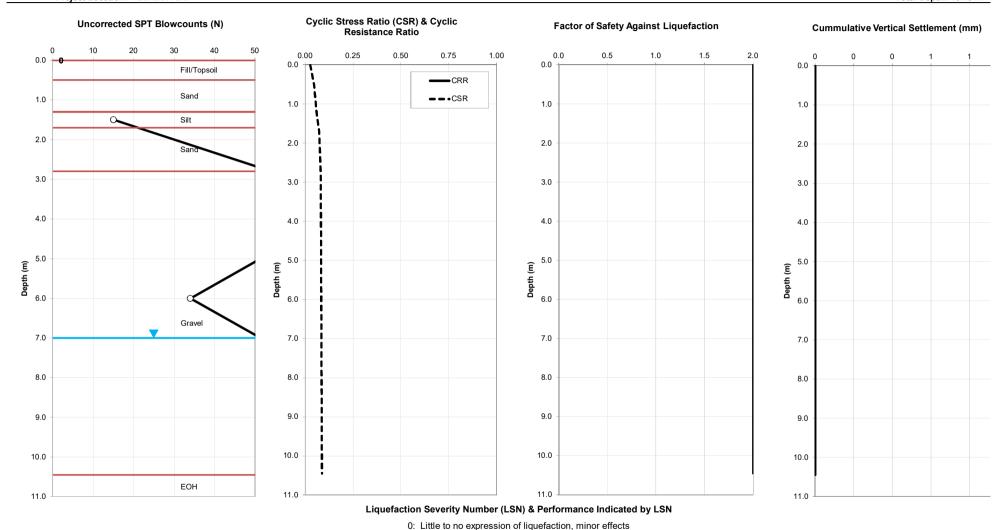
Vertical Settlement Method: Ishihara & Yoshimine (1992)

Project Name: Subdivision Development

Borehole: BH_02

Project Location: Yaldhurst Park

Total Depth: 10.45 m



ENGEO Ref: 15518.000.000 Author: HF Reviewer: DEB Date: 1/12/2018 Design Case: SLS Case 1 Magnitude: 7.5 PGA (g): 0.13

Analysis Method: Idriss and Boulanger (2008,2010)

Groundwater Depth (m): 7
Probability of Liquefaction Curve Used: 16 %

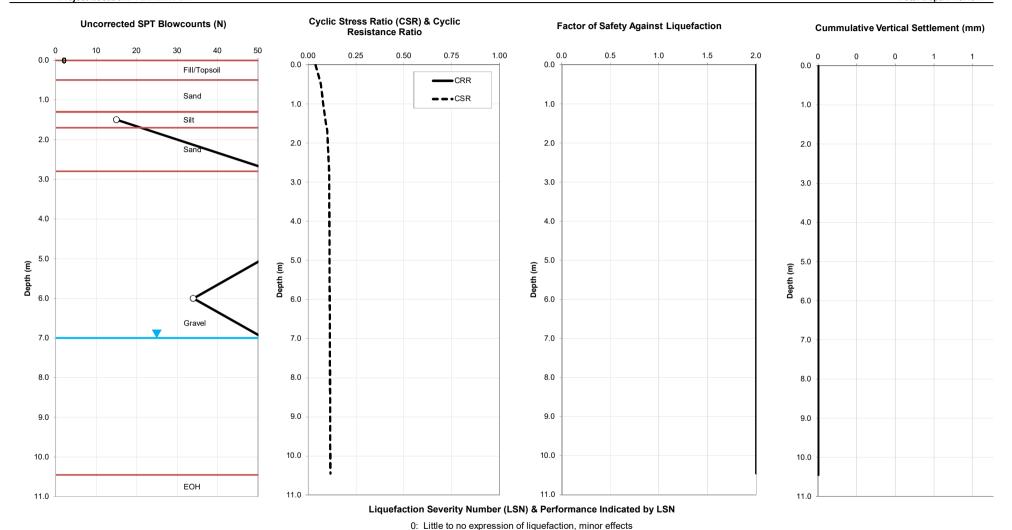
Vertical Settlement Method: Ishihara & Yoshimine (1992)

Project Name: Subdivision Development

Borehole: BH_02

Project Location: Yaldhurst Park

Total Depth: 10.45 m



ENGEO Ref: 15518.000.000 Author: HF Reviewer: DEB

viewer: DEB Date: 1/12/2018 Design Case: SLS Case 2 Magnitude: 6 PGA (g): 0.19

Analysis Method: Idriss and Boulanger (2008,2010)

Groundwater Depth (m): 7
Probability of Liquefaction Curve Used: 16 %

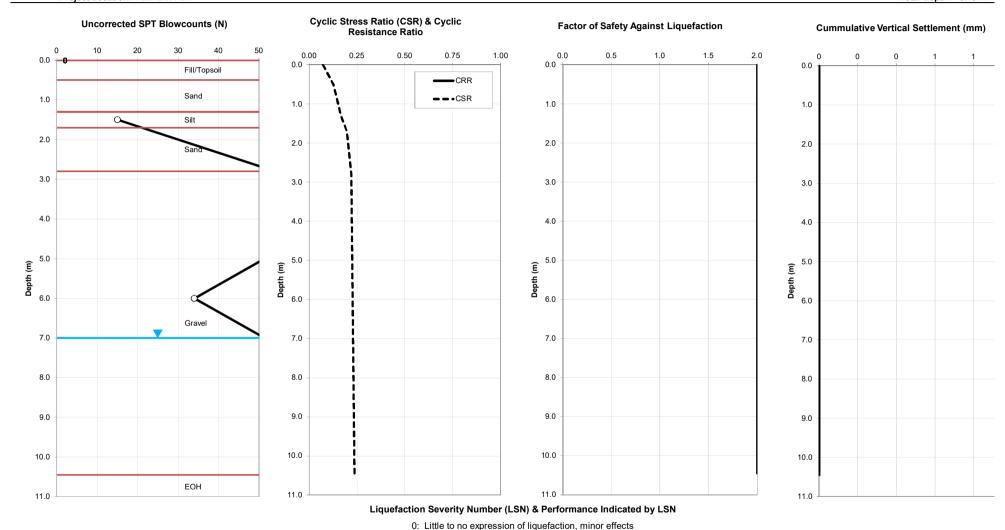
Vertical Settlement Method: Ishihara & Yoshimine (1992)

Project Name: Subdivision Development

Borehole: BH_02

Project Location: Yaldhurst Park

Total Depth: 10.45 m



ENGEO Ref: 15518.000.000 Author: HF

Reviewer: DEB Date: 1/12/2018 Design Case: ULS Magnitude: 7.5 PGA (g): 0.35

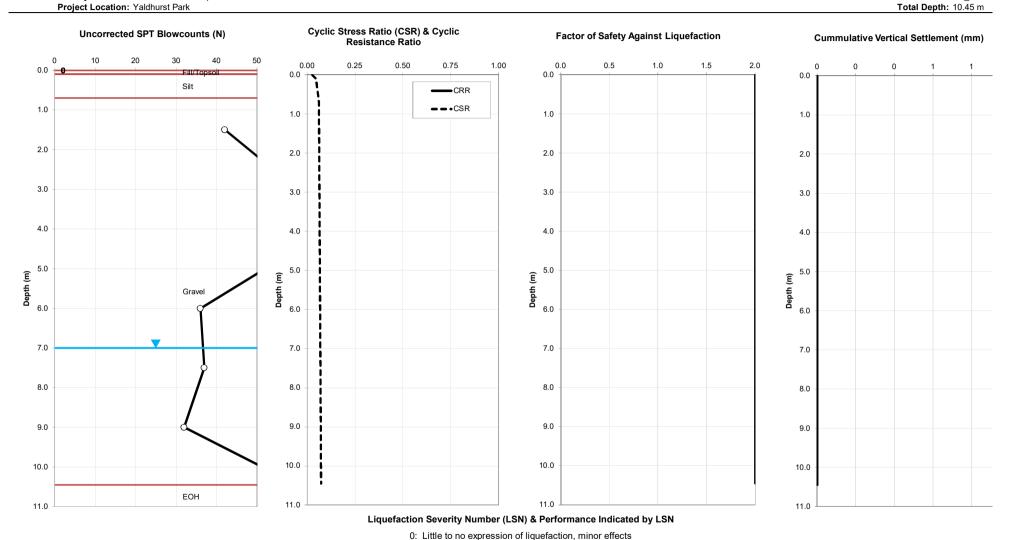
Analysis Method: Idriss and Boulanger (2008,2010)

Groundwater Depth (m): 7
Probability of Liquefaction Curve Used: 16 %

Vertical Settlement Method: Ishihara & Yoshimine (1992)

Borehole: BH 03

Project Name: Subdivision Development Project Location: Yaldhurst Park



ENGEO Ref: D3566132 Author: HF Reviewer: DEB Date: 1/12/2018

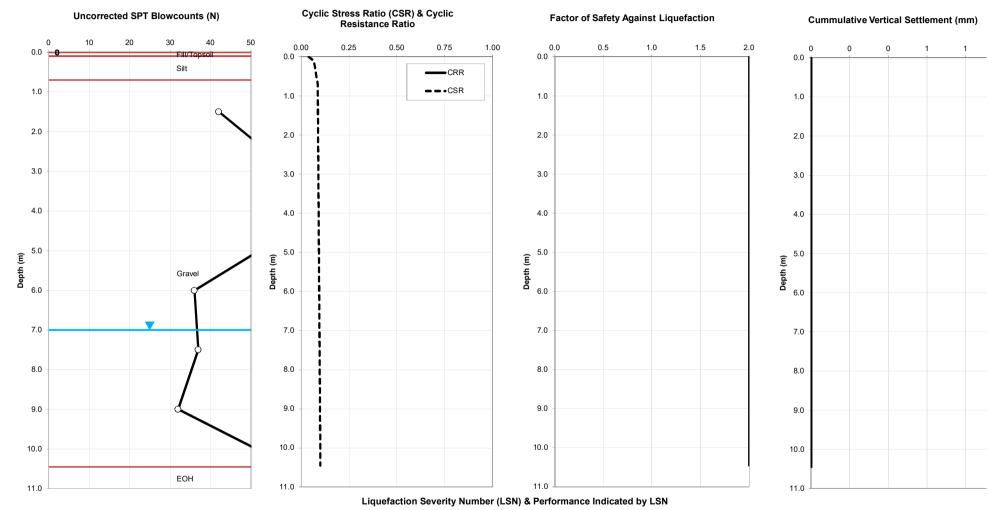
Design Case: SLS Case 1 Magnitude: 7.5 PGA (g): 0.13

Analysis Method: Idriss and Boulanger (2008,2010)

Groundwater Depth (m): 7 Probability of Liquefaction Curve Used: 16 %

Vertical Settlement Method: Ishihara & Yoshimine (1992)

Project Name: Subdivision Development Borehole: BH 03 Total Depth: 10.45 m Project Location: Yaldhurst Park



0: Little to no expression of liquefaction, minor effects

ENGEO Ref: D3566132 Author: HF Reviewer: DEB Date: 1/12/2018

Design Case: SLS Case 2 Magnitude: 6 PGA (g): 0.19

Analysis Method: Idriss and Boulanger (2008,2010)

Groundwater Depth (m): 7 Probability of Liquefaction Curve Used: 16 %

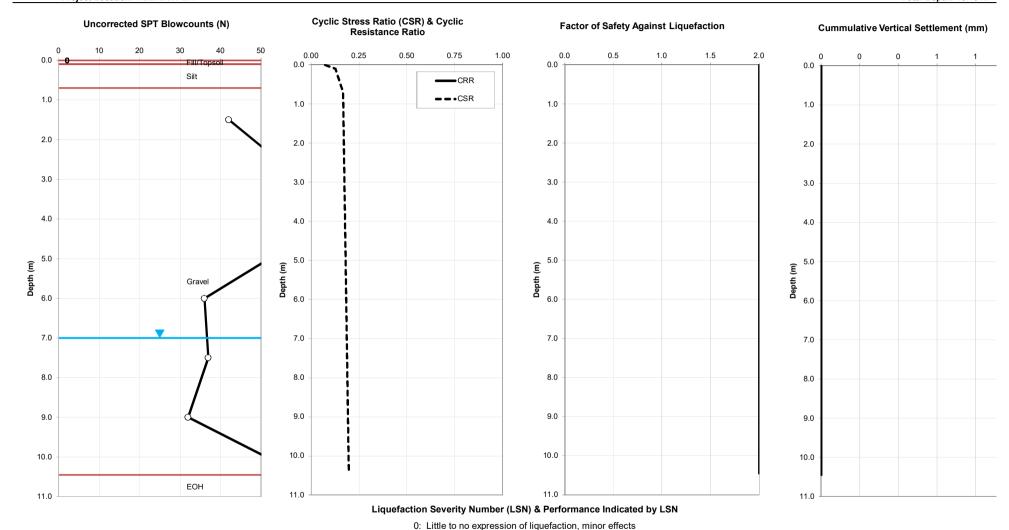
Vertical Settlement Method: Ishihara & Yoshimine (1992)

Project Name: Subdivision Development

Borehole: BH_03

Project Location: Yaldhurst Park

Total Depth: 10.45 m



ENGEO Ref: D3566132 Author: HF Reviewer: DEB Date: 1/12/2018 Design Case: ULS Magnitude: 7.5 PGA (g): 0.35

Analysis Method: Idriss and Boulanger (2008,2010)

Groundwater Depth (m): 7
Probability of Liquefaction Curve Used: 16 %

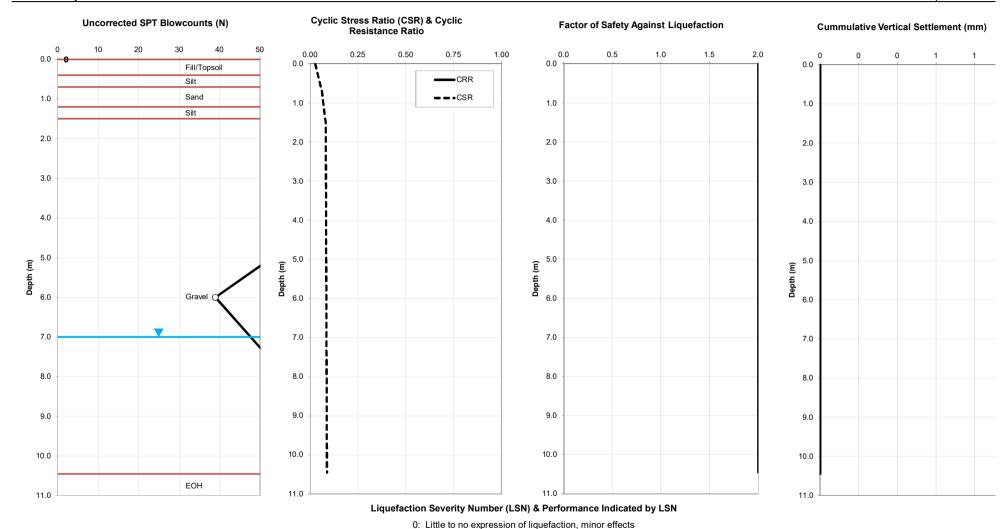
Vertical Settlement Method: Ishihara & Yoshimine (1992)

Project Name: Subdivision Development

Borehole: BH_04

Project Location: Yaldhurst Park

Total Depth: 10.45 m



ENGEO Ref: 15518.000.000 Author: HF Reviewer: DEB

viewer: DEB Date: 1/12/2018 Design Case: SLS Case 1 Magnitude: 7.5 PGA (g): 0.13

Analysis Method: Idriss and Boulanger (2008,2010)

Groundwater Depth (m): 7
Probability of Liquefaction Curve Used: 16 %

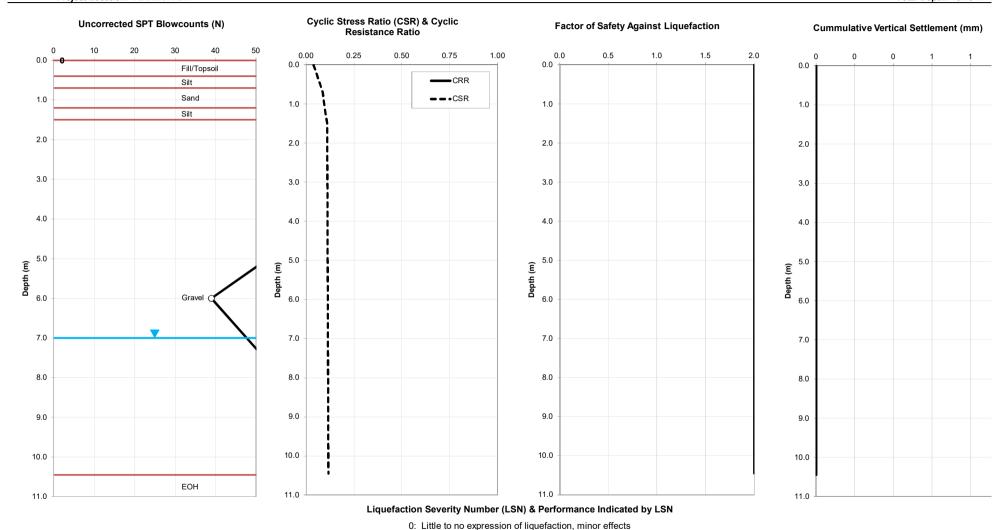
Vertical Settlement Method: Ishihara & Yoshimine (1992)

Project Name: Subdivision Development

Borehole: BH_04

Project Location: Yaldhurst Park

Total Depth: 10.45 m



ENGEO Ref: 15518.000.000 Author: HF Reviewer: DEB Date: 1/12/2018 Design Case: SLS Case 2 Magnitude: 6 PGA (g): 0.19

Analysis Method: Idriss and Boulanger (2008,2010)

Groundwater Depth (m): 7
Probability of Liquefaction Curve Used: 16 %

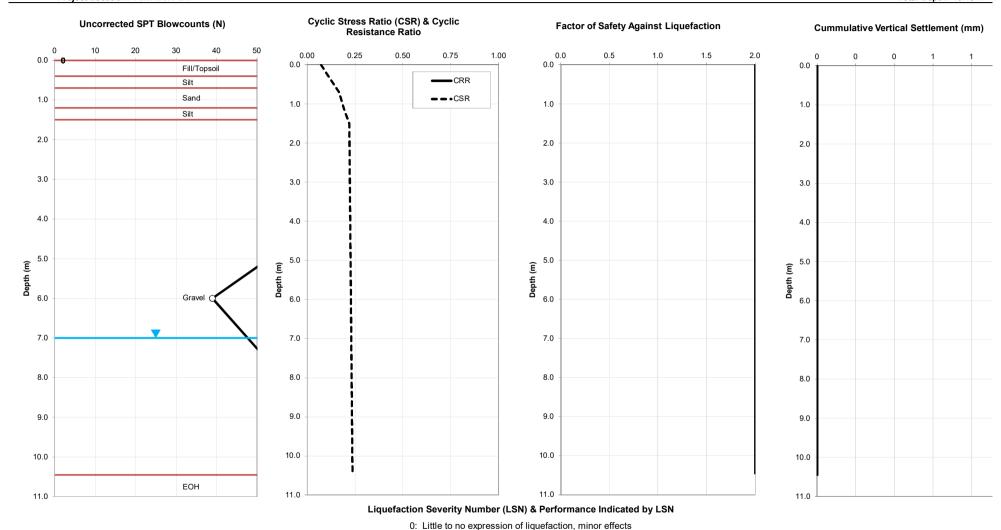
Vertical Settlement Method: Ishihara & Yoshimine (1992)

Project Name: Subdivision Development

Borehole: BH_04

Project Location: Yaldhurst Park

Total Depth: 10.45 m



ENGEO Ref: 15518.000.000 Author: HF Reviewer: DEB Date: 1/12/2018 Design Case: ULS Magnitude: 7.5 PGA (g): 0.35

Analysis Method: Idriss and Boulanger (2008,2010)

Groundwater Depth (m): 7
Probability of Liquefaction Curve Used: 16 %

Vertical Settlement Method: Ishihara & Yoshimine (1992)